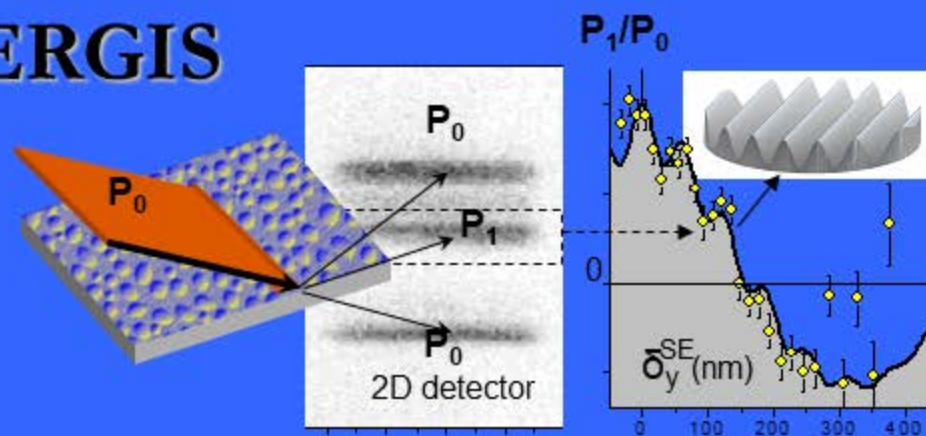


# SPIN-ECHO CODING OF THE MOMENTUM TRANSFER IN GRAZING INCIDENCE SCATTERING

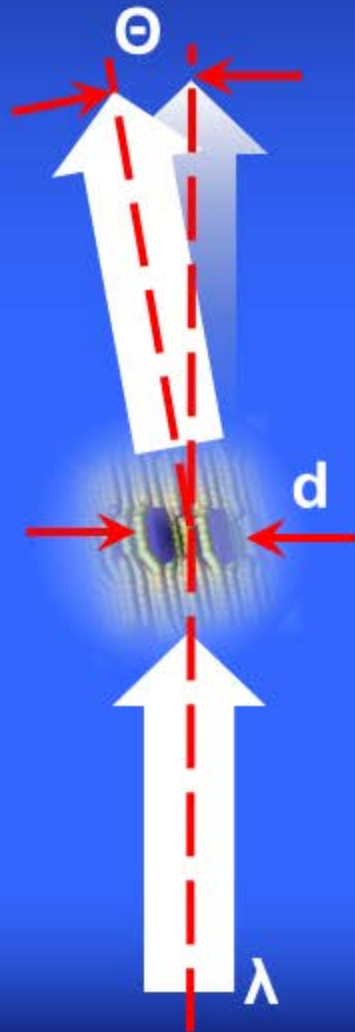
Alexei Vorobiev  
Uppsala University

**SERGIS**



# FORMULATION OF THE PROBLEM

Neutron scattering uses Bragg's law to measure a distance  $d$  within the sample



$$\lambda = 2d \sin\Theta$$

if  $d \gg \lambda \Rightarrow \Theta$  is small

- $\Rightarrow$  to measure small  $\Theta$  one has to collimate both incident and scattered beams
- $\Rightarrow$  measured intensity will be very low
- $\Rightarrow$  one should try to find a way to measure small angles without tightening of the beam

## Proposed solution:

use spin-echo encoding of the momentum transfer

depolarization of the beam is measured instead of the scattering angle

almost no collimation of the neutron beam is need

**structural information about the sample is obtained in real space**

# LARMOR PRECESSION

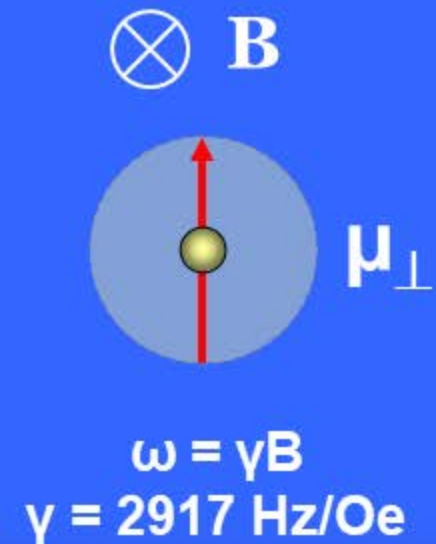
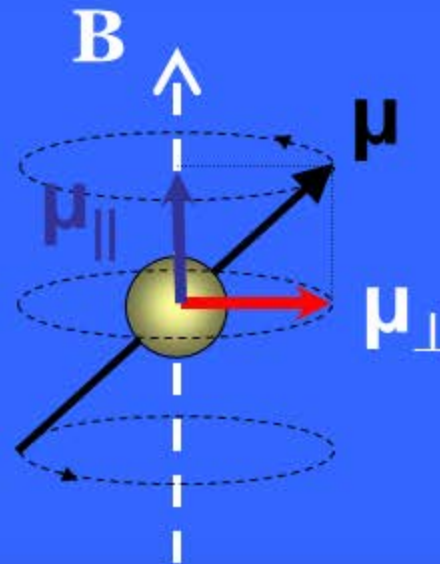
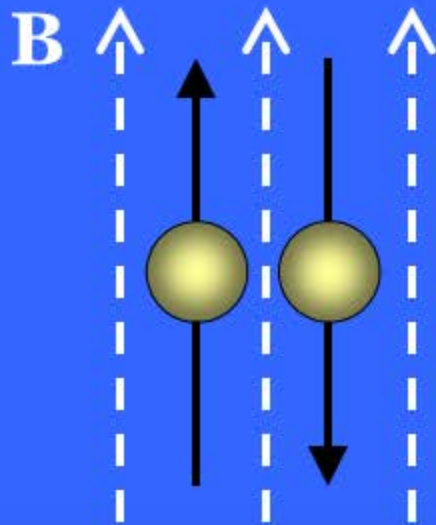
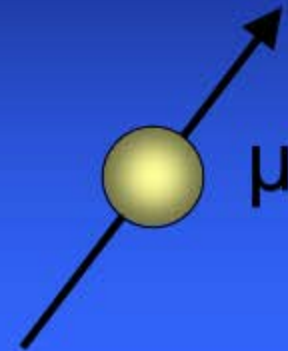
Neutron properties:

Mass  $m=1.674928(1)\cdot 10^{-27}$  kg

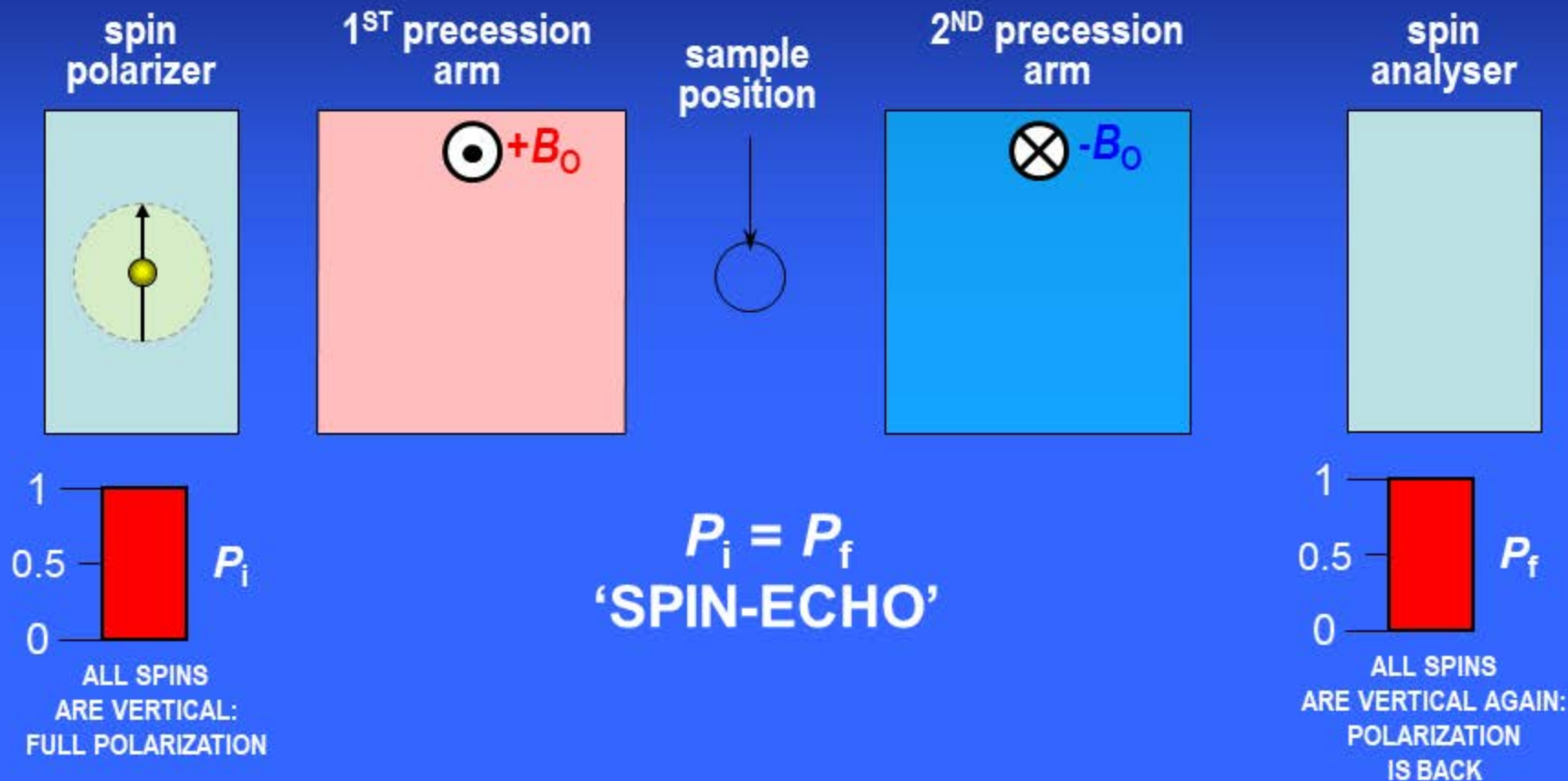
Spin  $s=\hbar/2$

Magnetic moment  $\mu=-9.649\cdot 10^{-27}$  JT<sup>-1</sup>

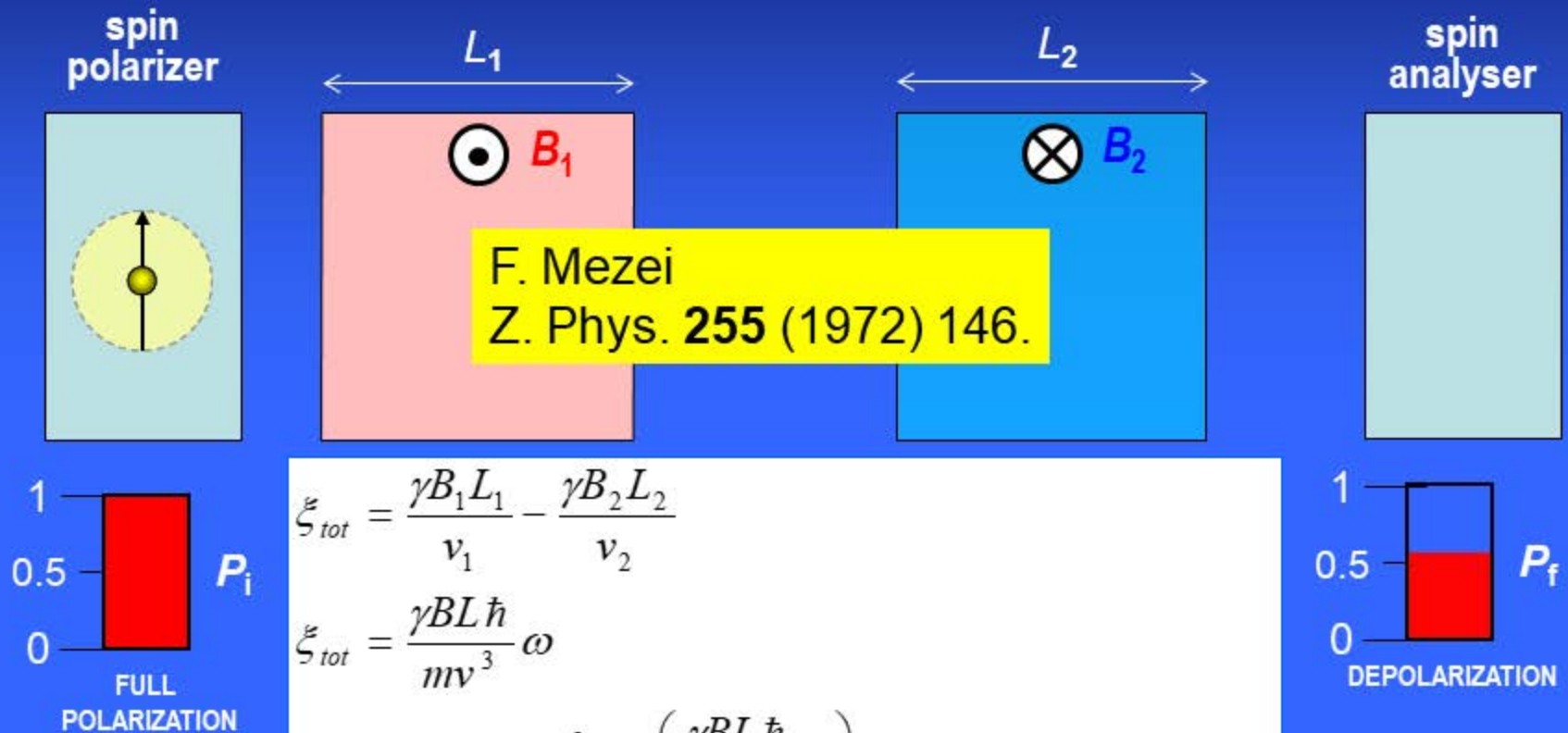
$\beta$ -decay lifetime  $\tau=886$  s



# CONVENTIONAL SPIN-ECHO FOR DYNAMIC STUDY



# INELASTIC SCATTERING



F. Mezei  
Z. Phys. **255** (1972) 146.

$$\xi_{tot} = \frac{\gamma B_1 L_1}{v_1} - \frac{\gamma B_2 L_2}{v_2}$$

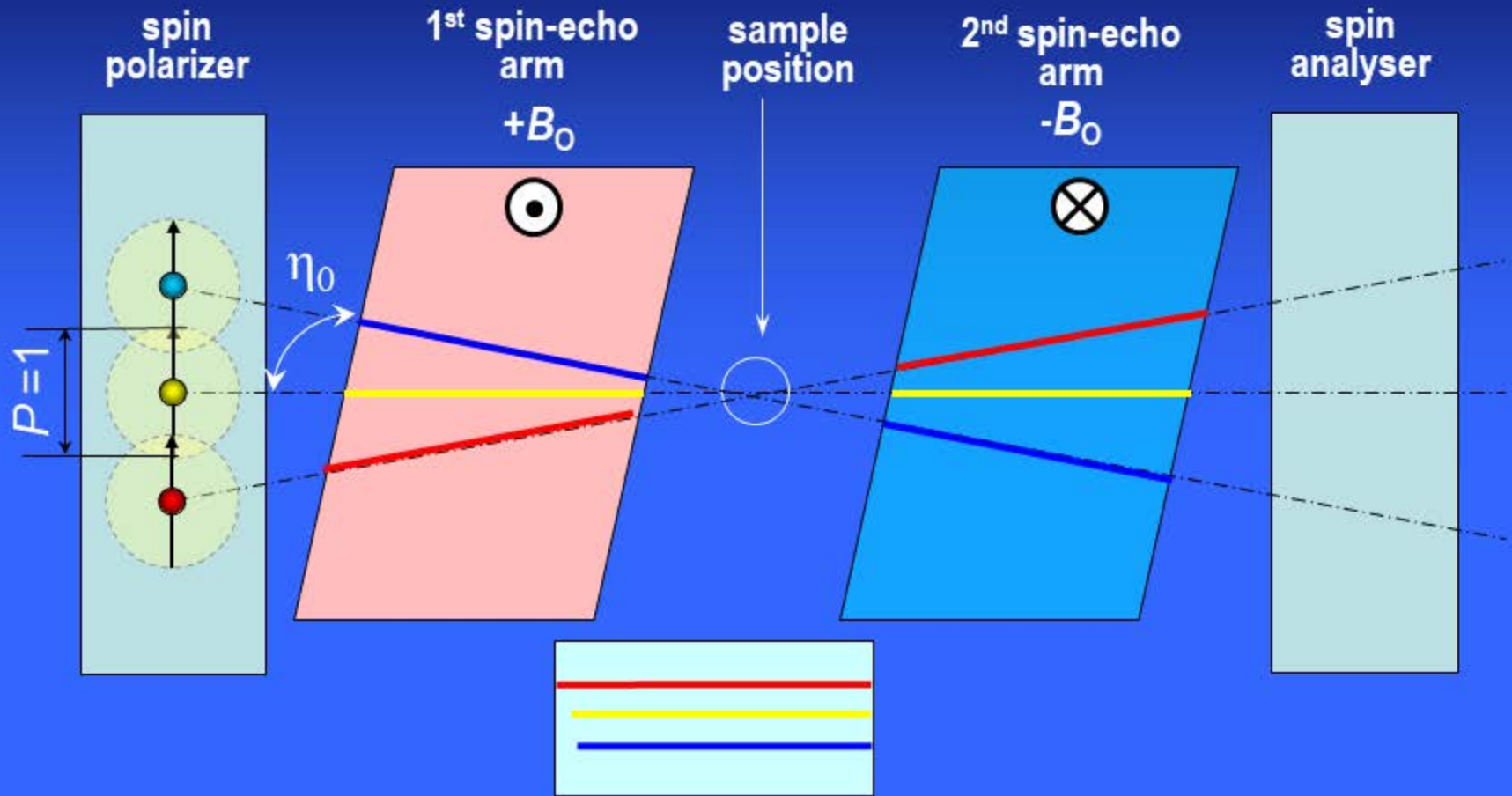
$$\xi_{tot} = \frac{\gamma B L \hbar}{m v^3} \omega$$

$$P = \langle \cos \xi \rangle = \frac{\int \cos \left( \frac{\gamma B L \hbar}{m v^3} \omega \right) S(q, \omega) d\omega}{\int S(q, \omega) d\omega} = S(q, t_{SE})$$

$$t_{SE} = \frac{\gamma B L \hbar}{m v^3} \propto \lambda^3$$

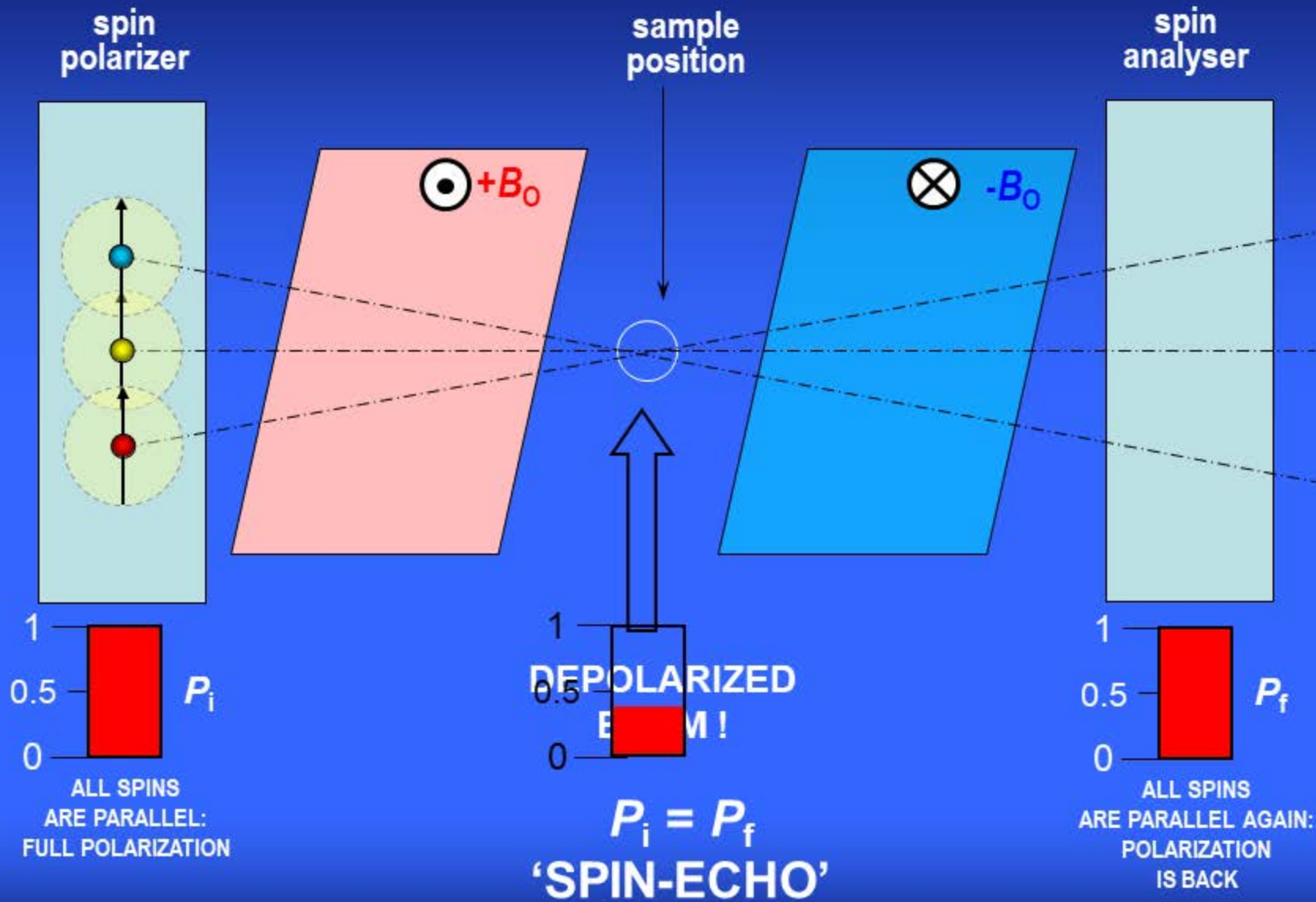
SPIN-ECHO (FOURIER) TIME

# INCLINED BORDERS



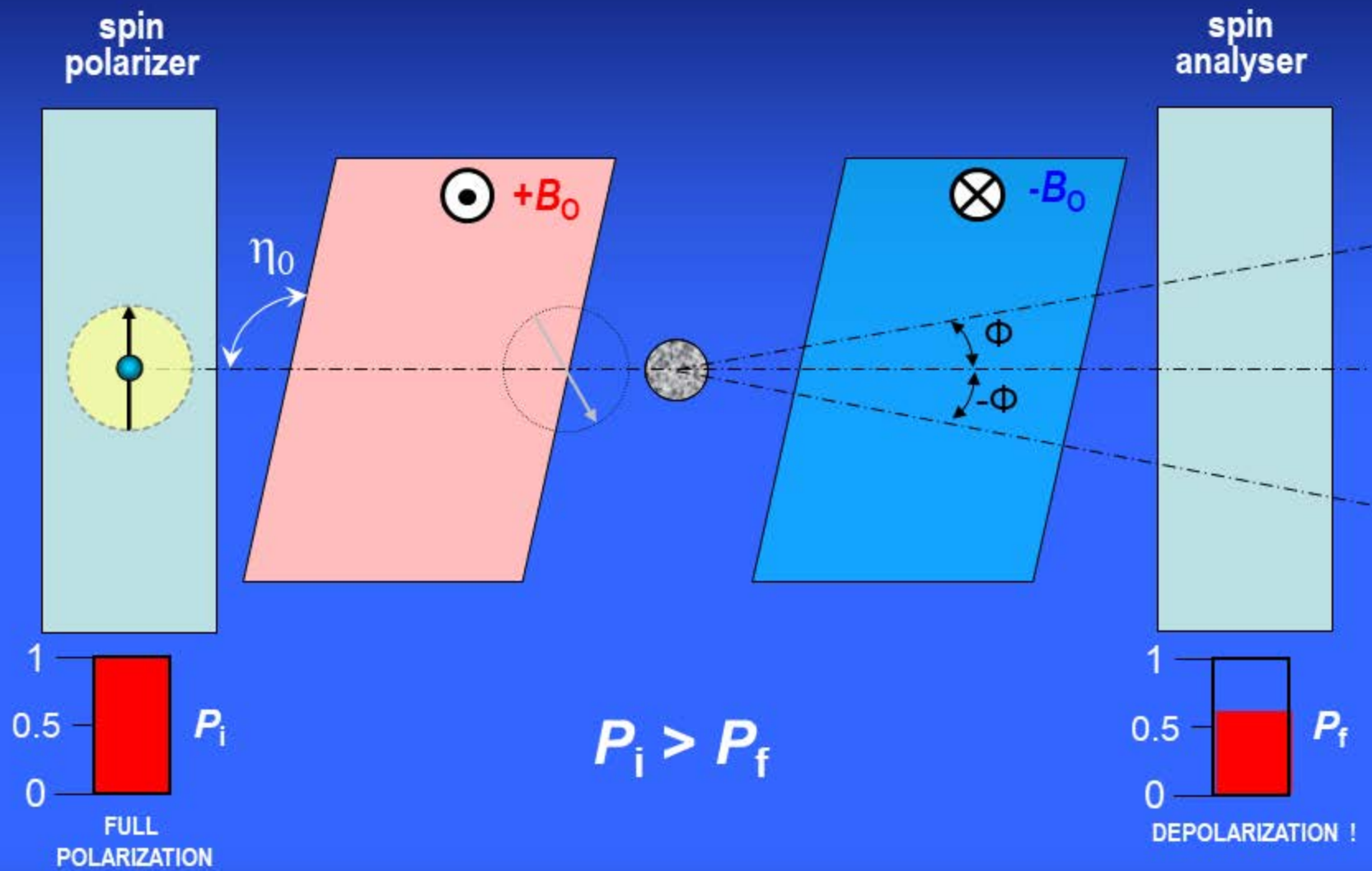
DIFFERENT PATH LENGTHS FOR  
THE DIFFERENT TRAJECTORIES !

# NO-SCATTERING CASE

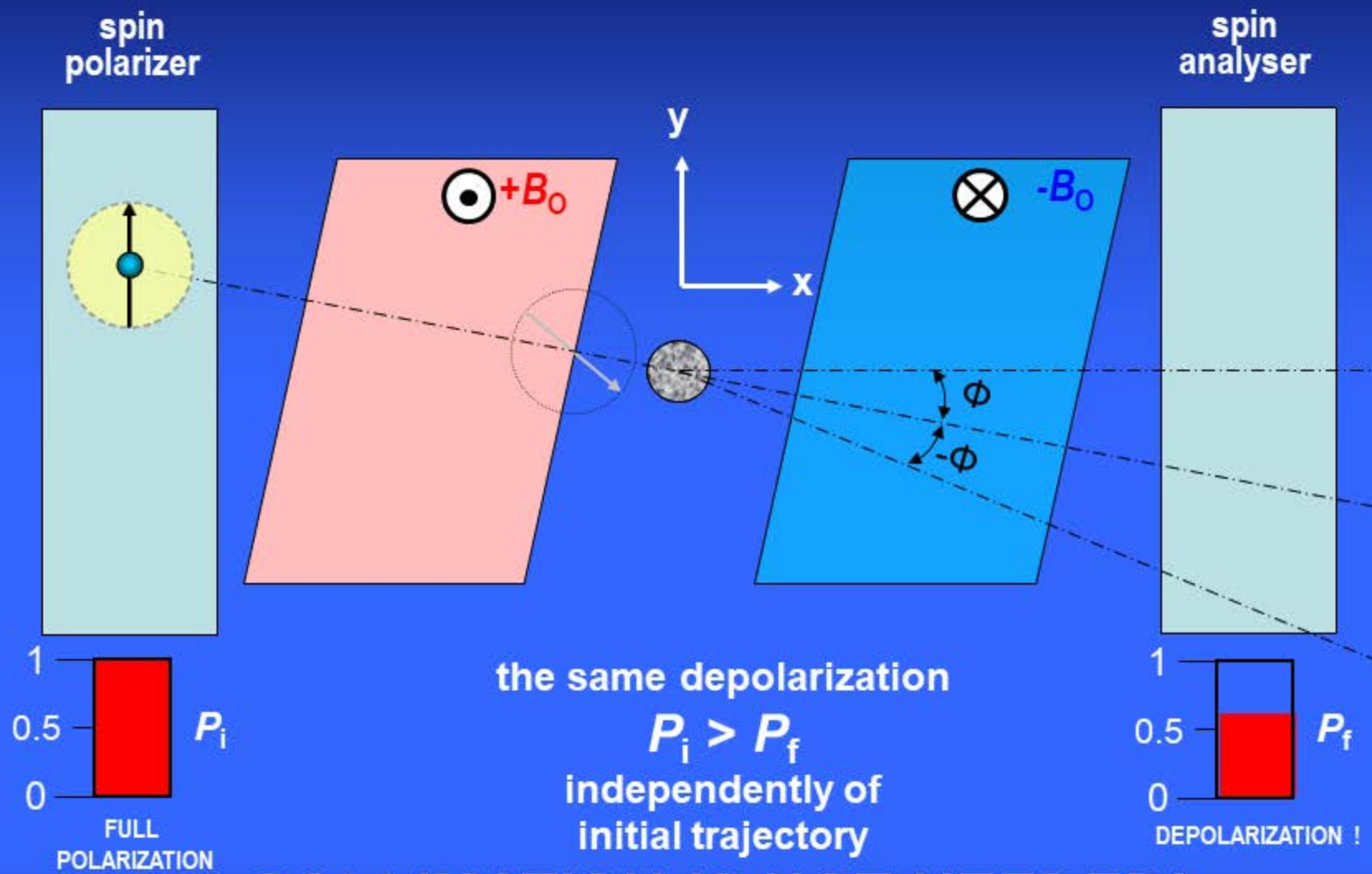




# SCATTERING BY THE SAMPLE

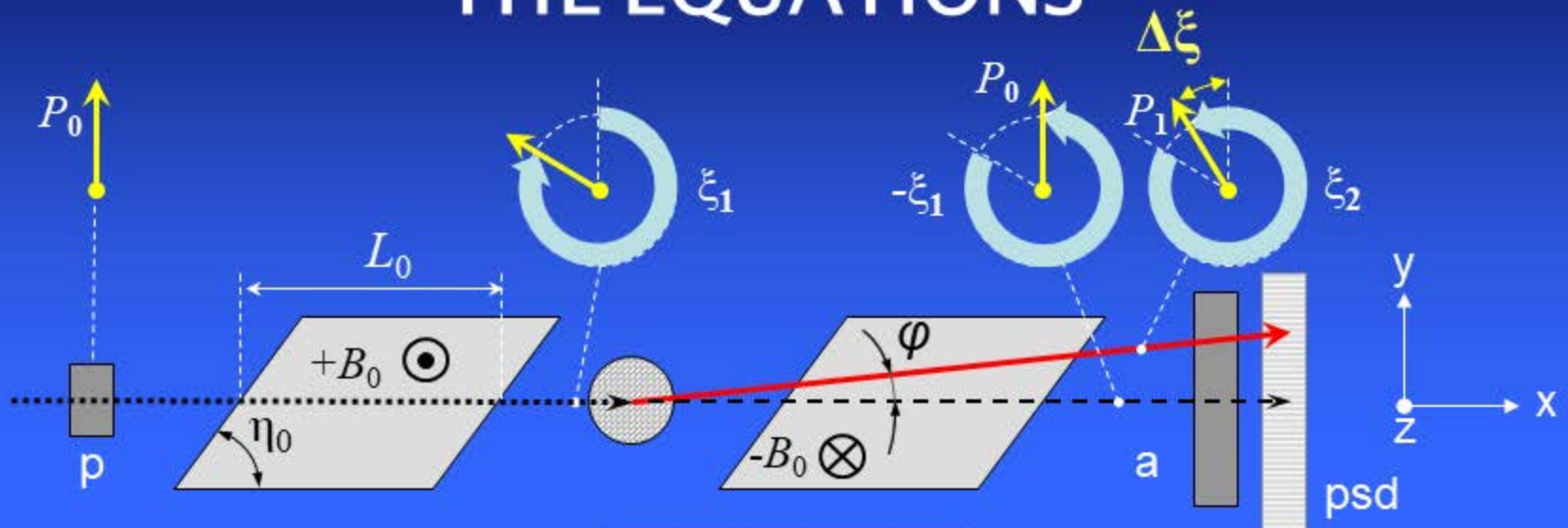


# SCATTERING BY THE SAMPLE



**COLLIMATION IS NOT NEEDED!**

# SPIN-ECHO ANGULAR ENCODING: THE EQUATIONS



$$P_1 = P_0 \cos \Delta \xi .$$

$$\Delta \xi = \xi_1 - \xi_2 = 2\pi \gamma_n B_0 \frac{L_0}{v} \left( 1 - \frac{1}{\cos \varphi + \sin \varphi \cot \eta_0} \right) \cong \left( 2\pi \gamma_n \frac{B_0 L_0}{v} \cot \eta_0 \right) \sin \varphi =$$

$$= \left( \frac{\gamma_n B_0 L_0 \lambda^2}{K} \cot \eta_0 \right) \left( \frac{2\pi}{\lambda} \sin \varphi \right) \equiv \delta_y^{\text{SE}} q_y$$

# SPIN-ECHO GIVES RESULTS IN REAL SPACE

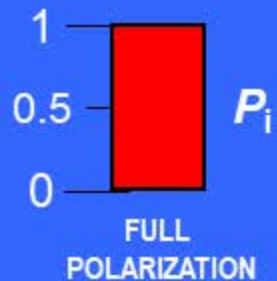
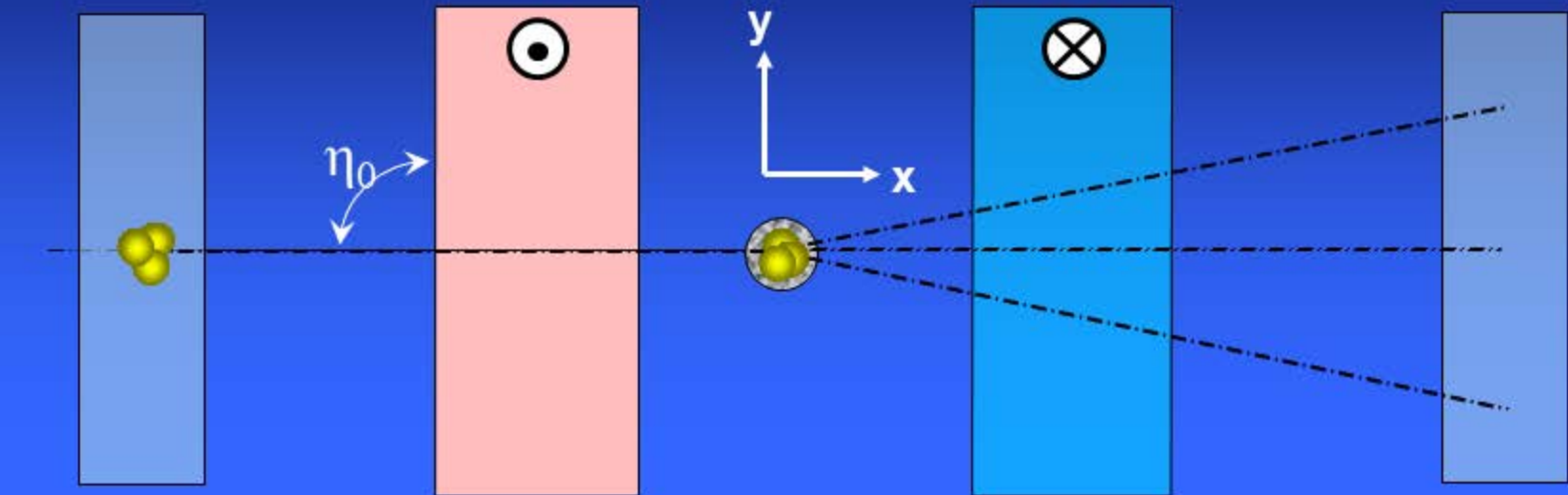
$$P_1 = P_0 \cos \Delta\xi.$$

$$\frac{P_1}{P_0} = \langle \cos \Delta\xi \rangle \propto \frac{\int_{\det} dq_y dq_z S(\mathbf{q}) \cos(\delta_y^{\text{SE}} q_y)}{\int_{\det} dq_y dq_z S(\mathbf{q})} = \int dx \Pi(x, y, 0) \equiv G(y),$$

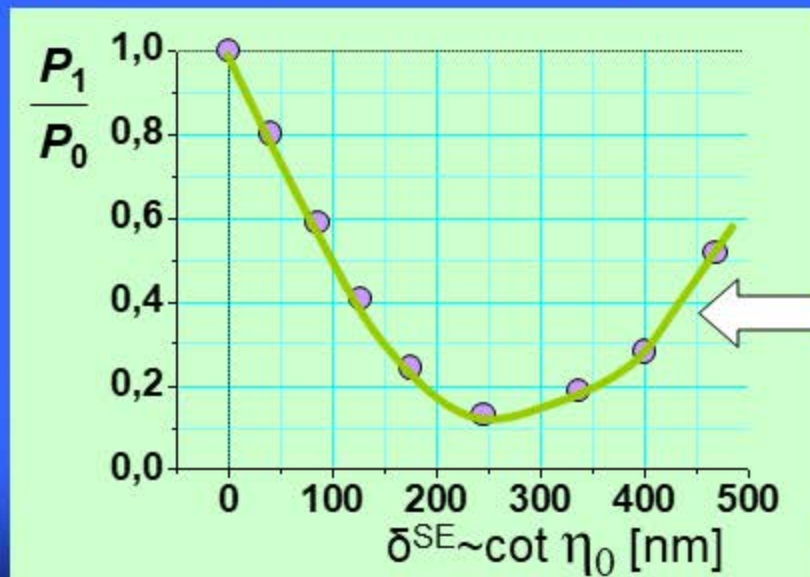
$$q_z = 0$$

$$\Pi(\mathbf{R}) = \int d\mathbf{r} \rho(\mathbf{r}) \rho(\mathbf{r} + \mathbf{R})$$

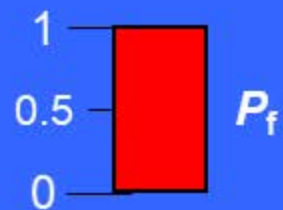
# EXPERIMENT: SE length scan



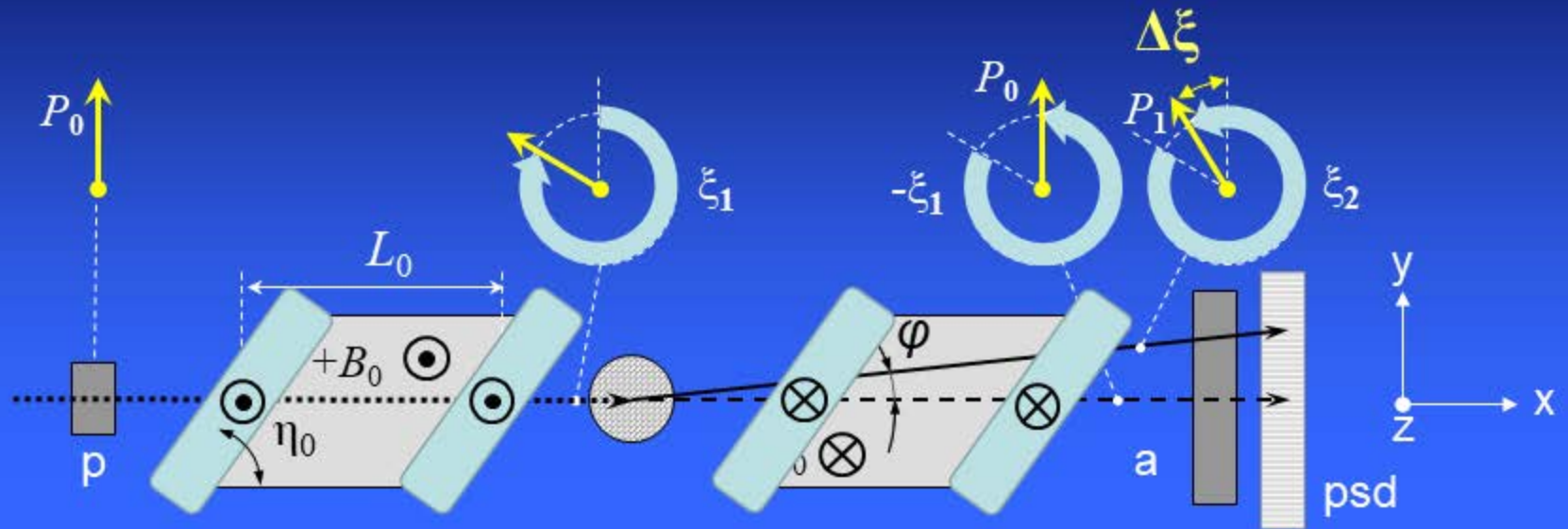
$$\left( \frac{\gamma_n B_0 L_0 \lambda^2}{K} \cot \eta_0 \right)$$



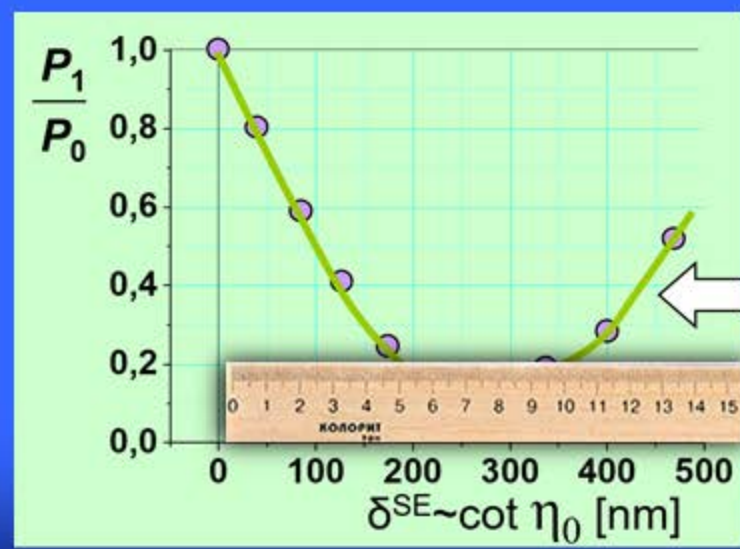
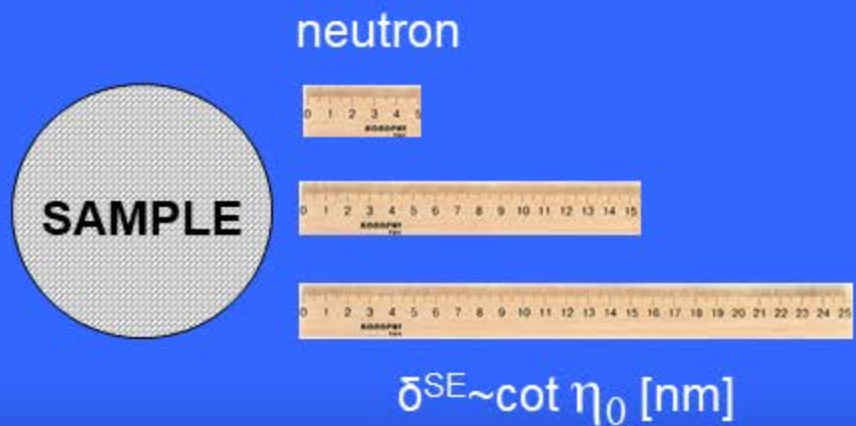
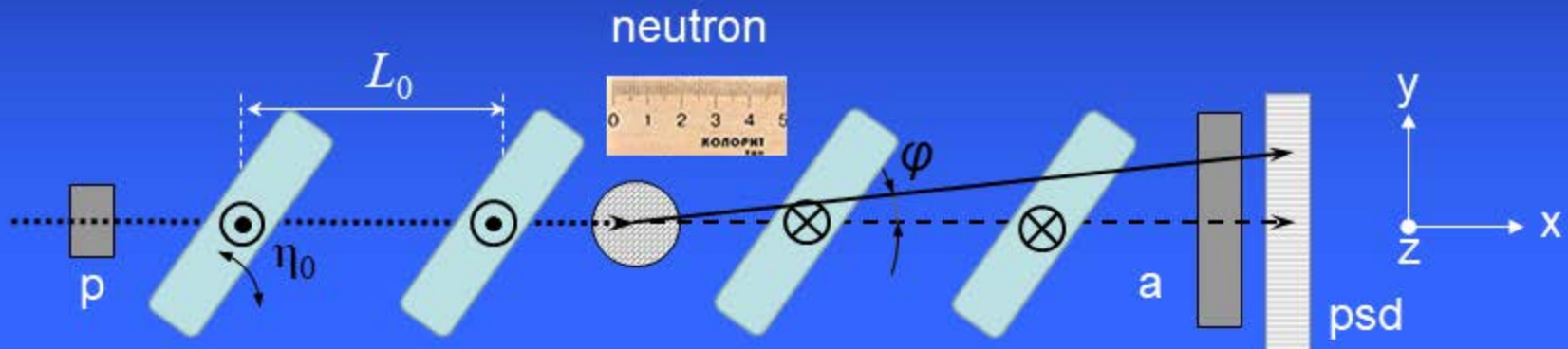
**REAL-SPACE  
CORRELATION  
FUNCTION**



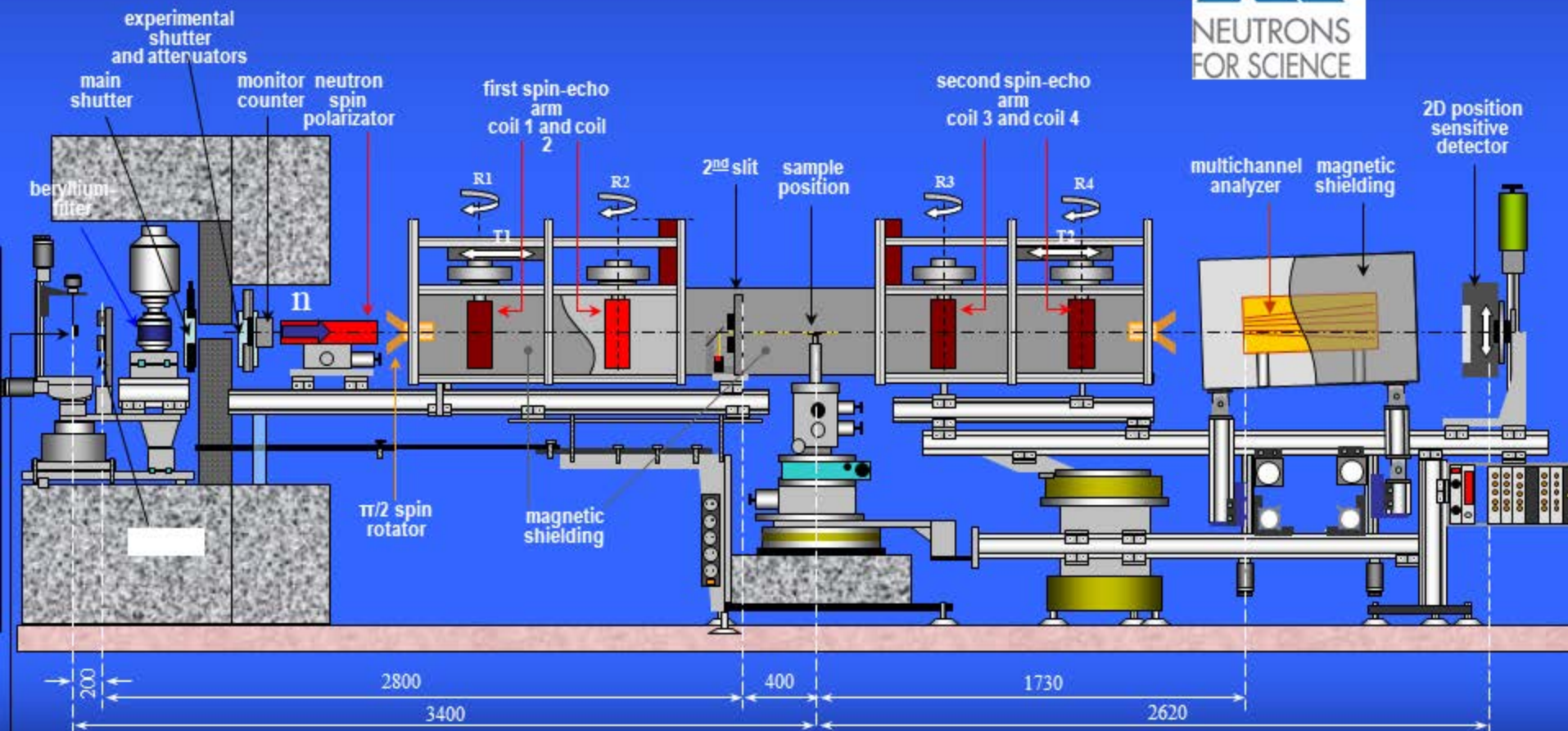
# SPIN-ECHO ANGULAR ENCODING



# SPIN-ECHO ANGULAR ENCODING:

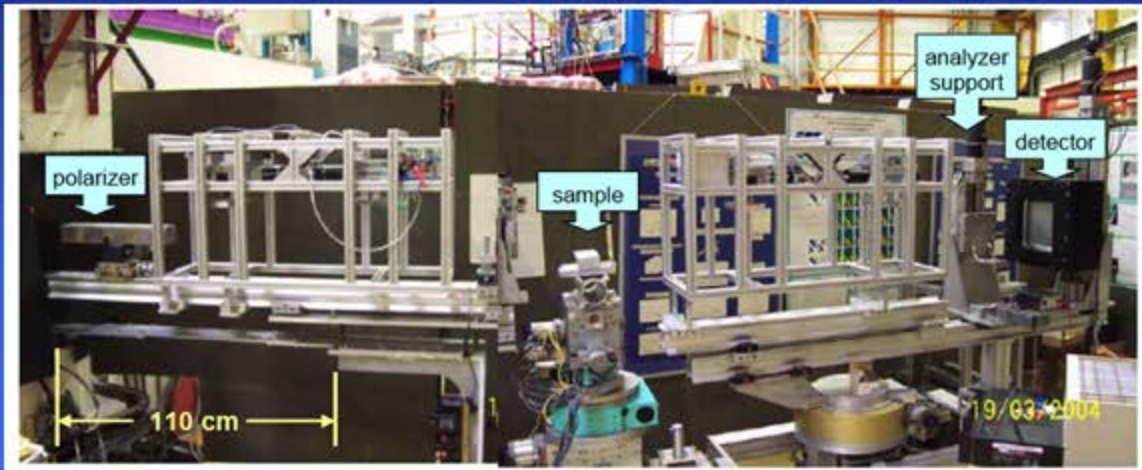


# EVA REFLECTOMETER TRANSFORMED INTO A SERGIS PROTOTYPE INSTRUMENT





# EVA DURING THE TRANSFORMATION TO SERGIS



Beam size 50x5mm

Wave numbers covered:

$1 \cdot 10^{-3} - 4 \cdot 10^{-2} \text{ \AA}^{-1}$

Max. SE time in classical configuration ( $\eta_0=0$ ) 0.07ns

**Max. SE length**

$$\delta = \left\{ \frac{\gamma_n B d \lambda \cdot \cot \Theta}{v} \right\} \quad \mathbf{4500 \text{ \AA}}$$

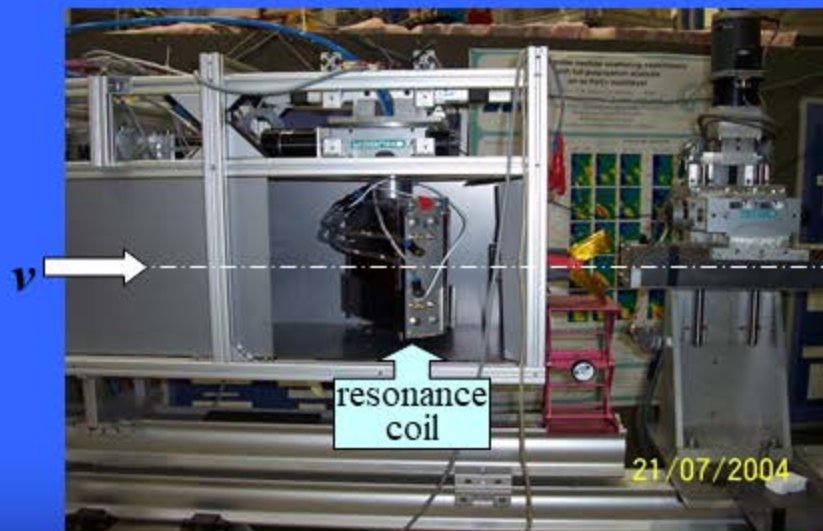
$\lambda$  (neutron wavelength) 5.5  $\text{\AA}$

$v$  (neutron velocity) 720 m/s

$\Theta$  (tilt of precession coil)  $50^\circ$

B (magnetic field in leg) 310G

d (length of precession leg) 50 cm

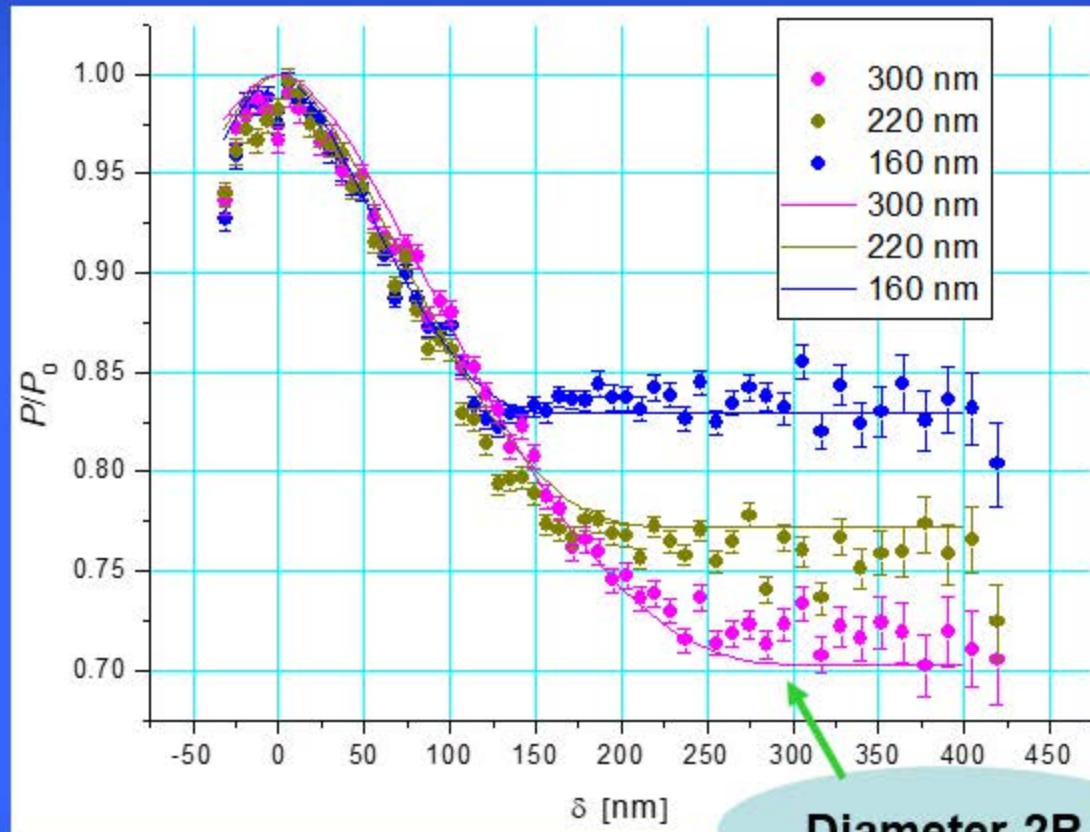


# EVA reflectometer transformed into a SERGIS prototype instrument

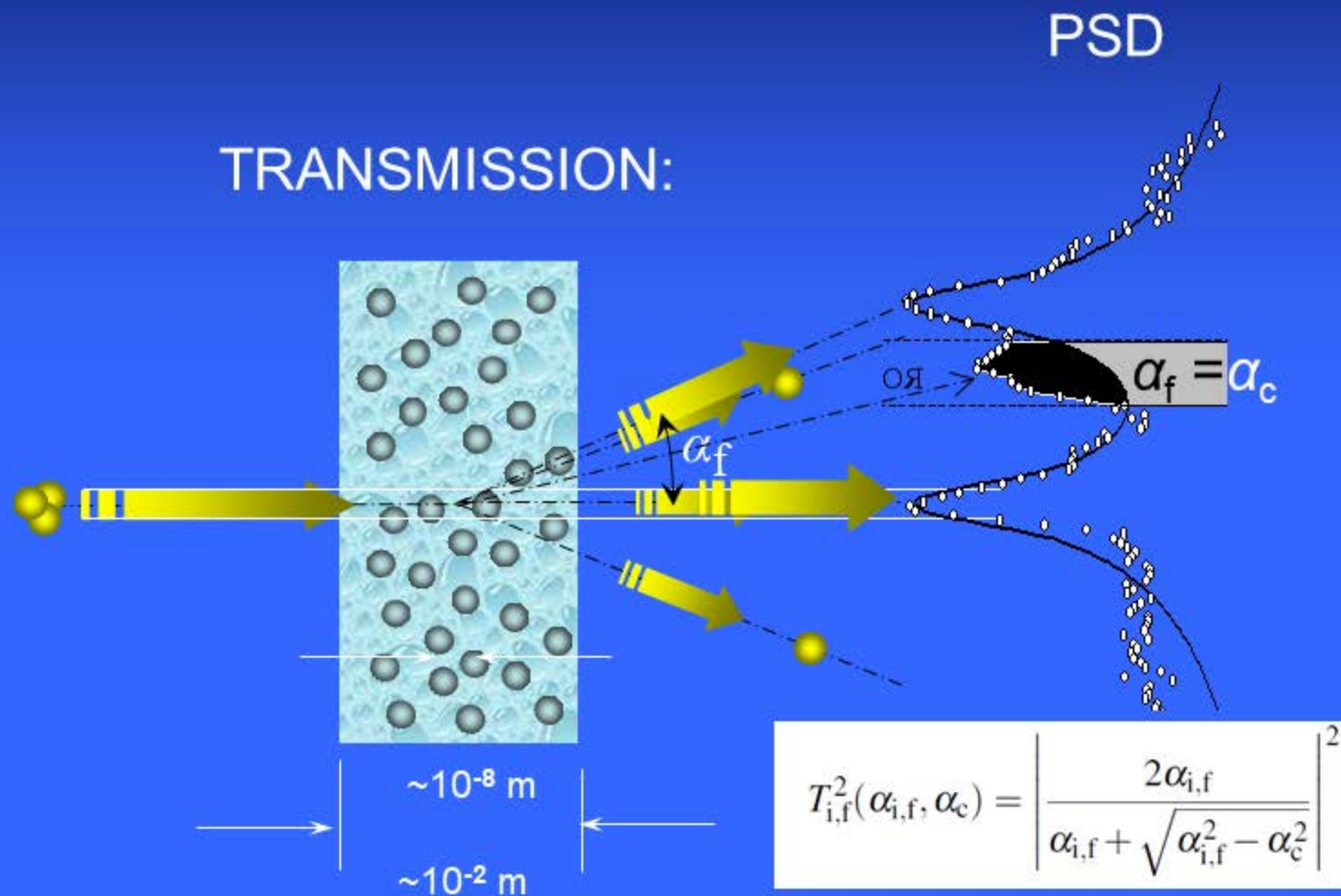


# Test SESANS experiments: polystyrene spheres

2.5% polystyrene balls in 3:1 D<sub>2</sub>O/H<sub>2</sub>O  
2mm thick cell



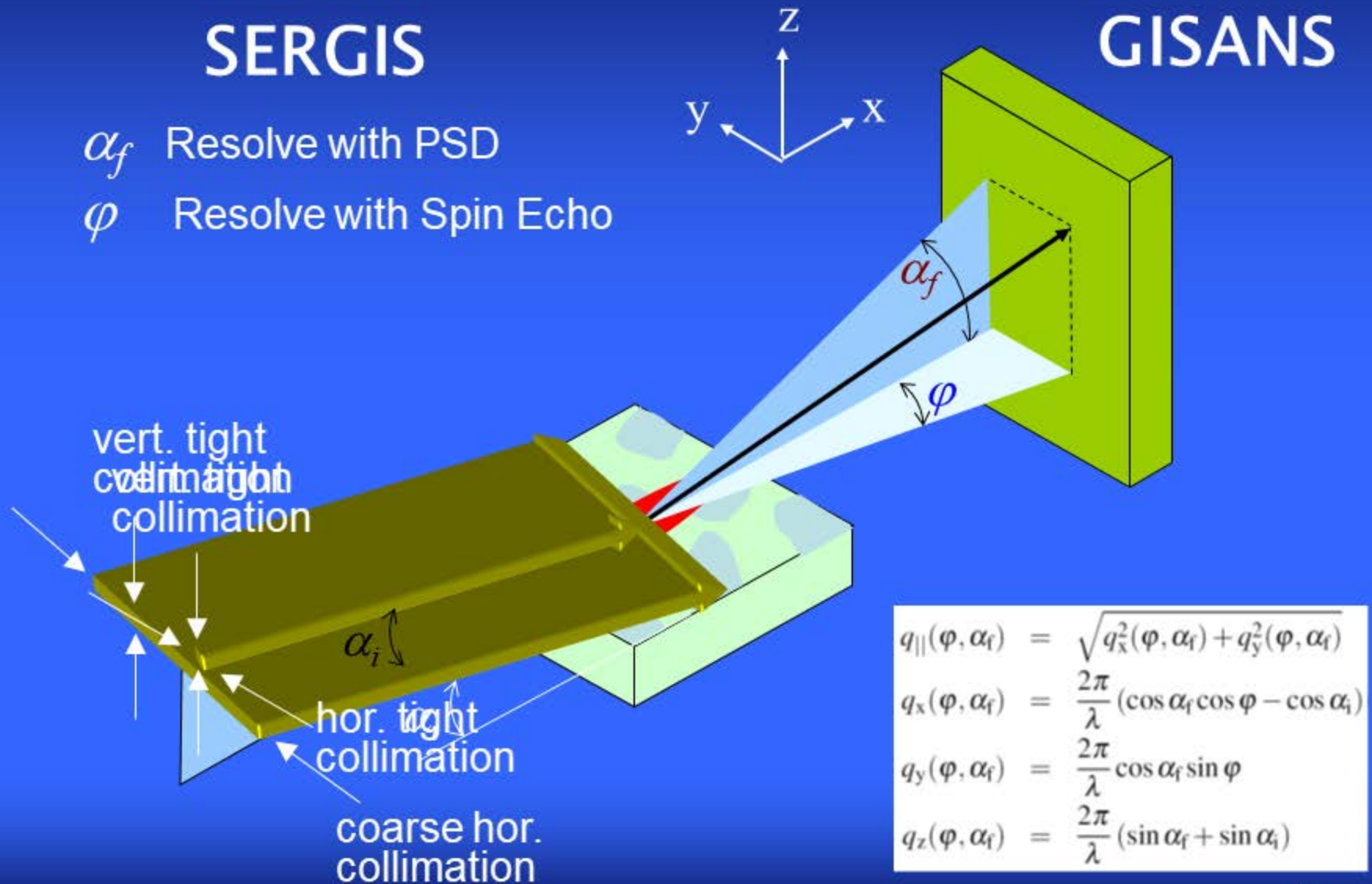
# GRAZING INCIDENCE



# SERGIS vs. GISANS

## SERGIS

- $\alpha_f$  Resolve with PSD
- $\varphi$  Resolve with Spin Echo

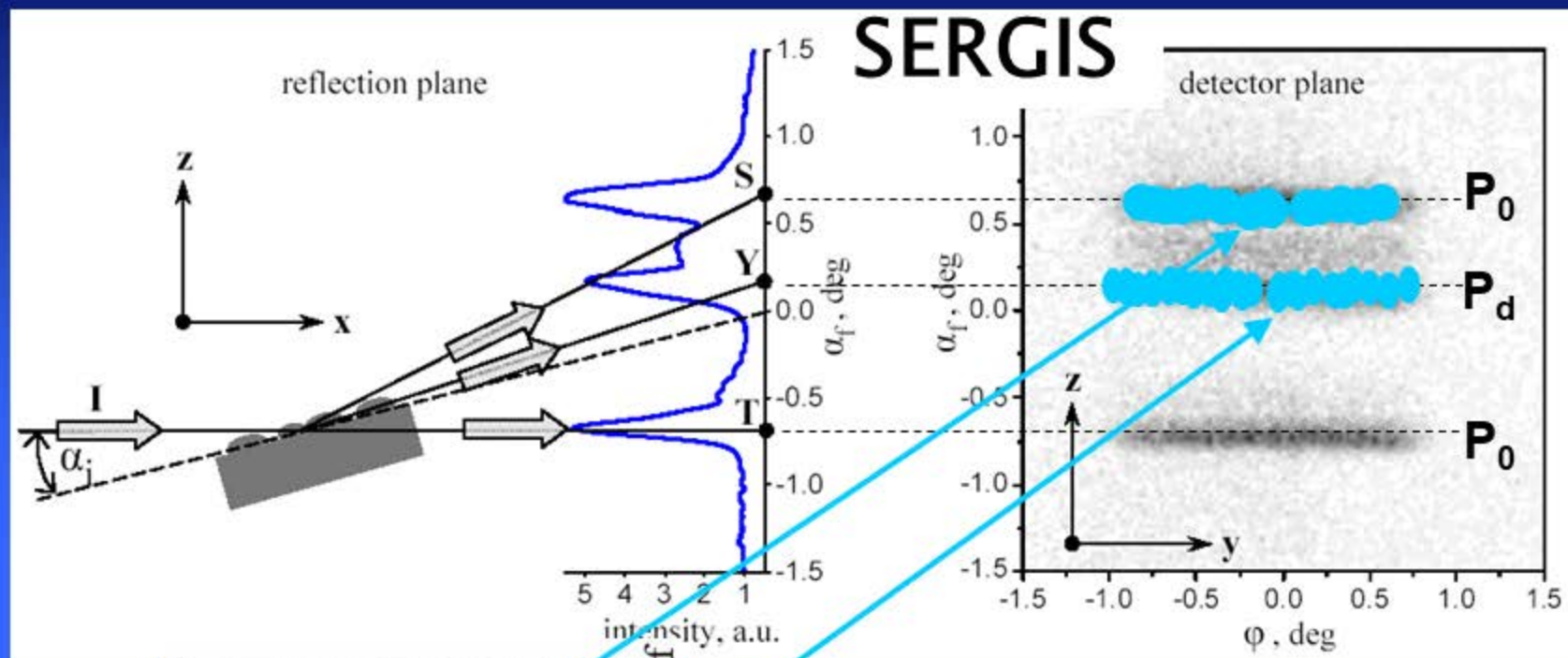


$$q_{||}(\varphi, \alpha_f) = \sqrt{q_x^2(\varphi, \alpha_f) + q_y^2(\varphi, \alpha_f)}$$

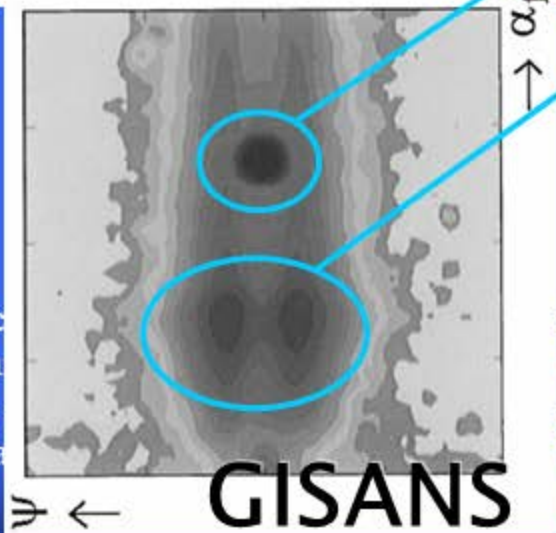
$$q_x(\varphi, \alpha_f) = \frac{2\pi}{\lambda} (\cos \alpha_f \cos \varphi - \cos \alpha_i)$$

$$q_y(\varphi, \alpha_f) = \frac{2\pi}{\lambda} \cos \alpha_f \sin \varphi$$

$$q_z(\varphi, \alpha_f) = \frac{2\pi}{\lambda} (\sin \alpha_f + \sin \alpha_i)$$



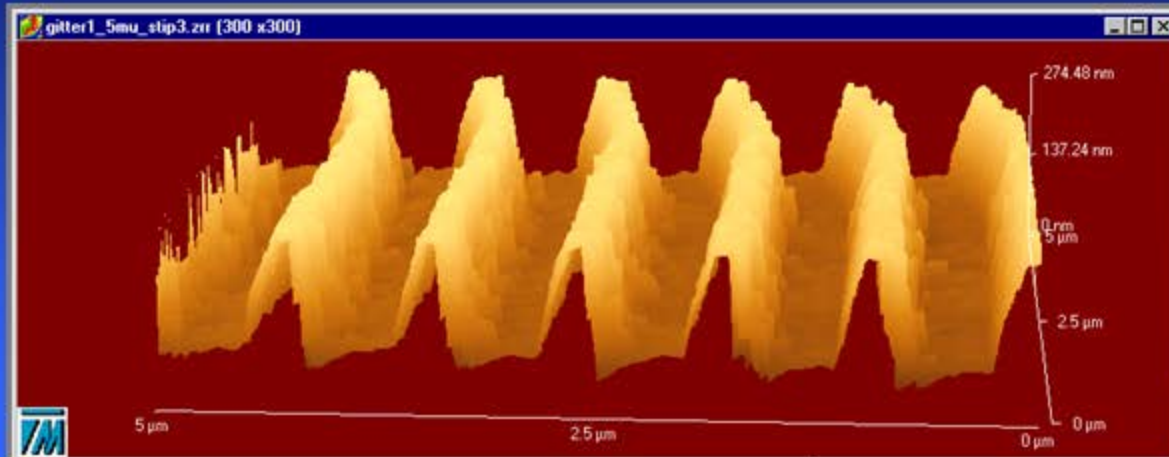
The sc  
transm  
Image  
beam a



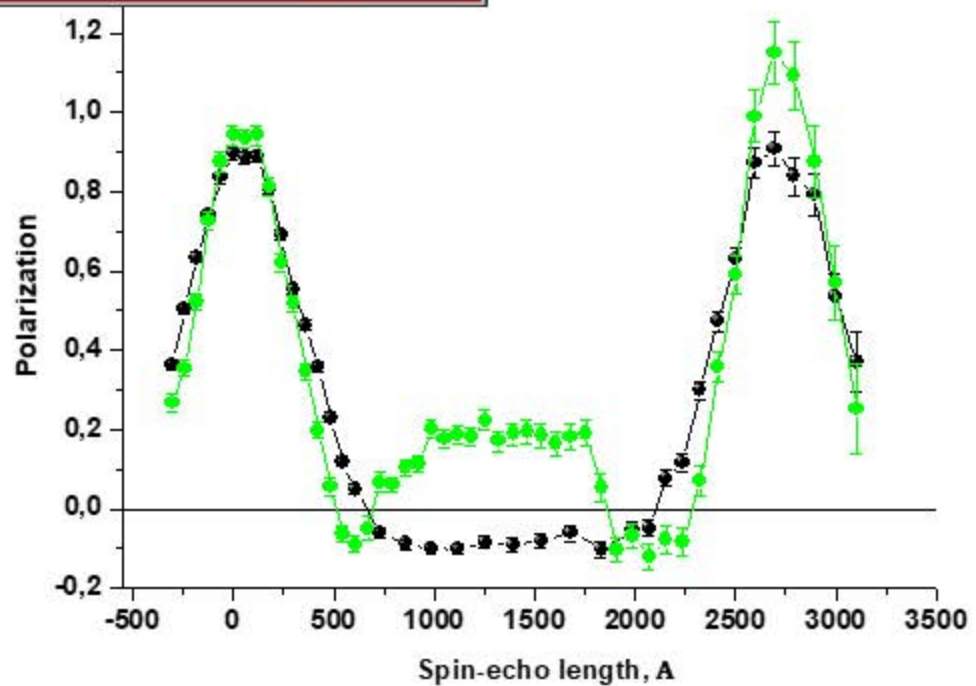
m (I) impinges on the sample surface at a shallow angle  $\alpha_i$ ;  
intensities are simultaneously recorded by PSD.

dimensional PSD during real experiment. The size of the incoming  
 $\lambda^2$ .

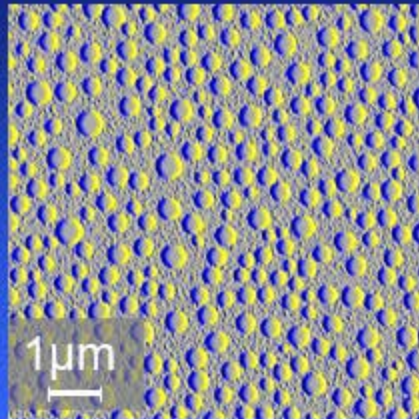
# OPTICAL DIFFRACTION GRATING



3600/mm  
2780 Å period

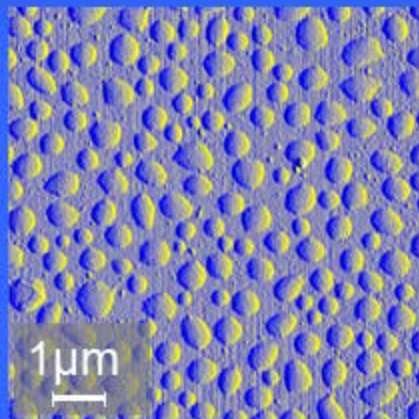


# SAMPLES: DEWETED POLYMER FILMS



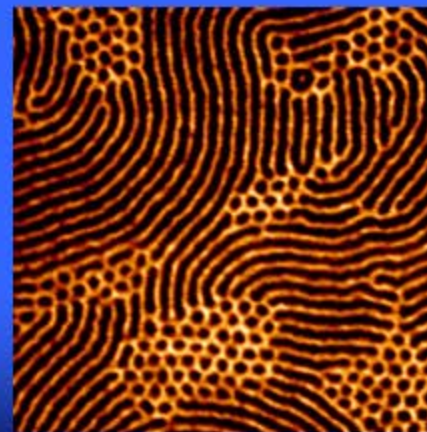
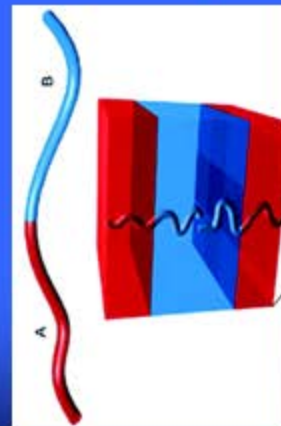
polymer blend

PpMS:dPS = 3:2  
polyparamethylstyrene  
d-polystyrene



diblock copolymer

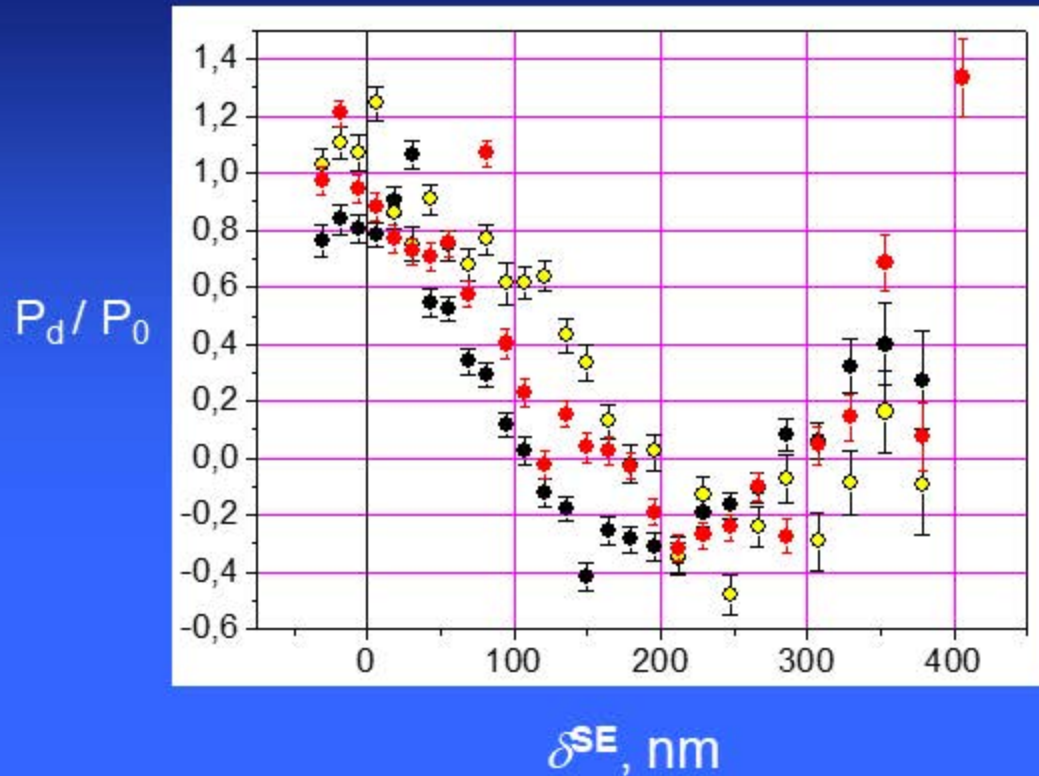
poly(styren-block-  
paramethylstyrene)  
P(S-b-pMS)



regular lamellar phase  
separation



# SERGIS EXPERIMENTAL DATA



- HOMOPOLYMER  
pancake-type  
droplets
- BLEND  
pancake-type  
droplets
- DIBLOCK  
'spherical'  
droplets

## DATA ANALYSIS via MODELING

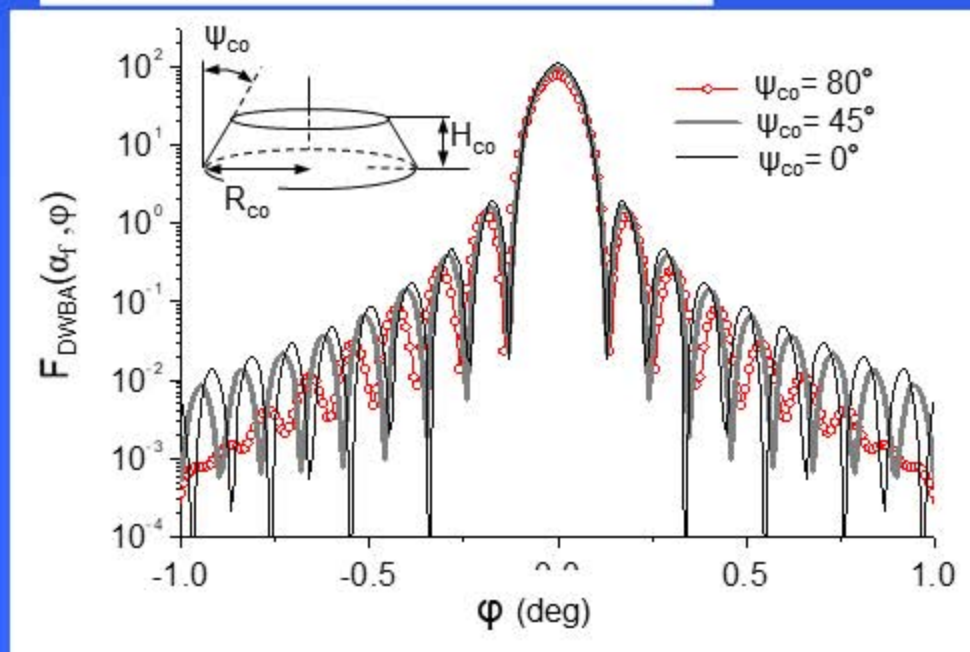
$$\frac{P_1}{P_0} = \langle \cos \Delta \xi \rangle \propto \frac{\int_{\text{det}} dq_y dq_z S(\mathbf{q}) \cos(\delta_y^{\text{SE}} q_y)}{\int_{\text{det}} dq_y dq_z S(\mathbf{q})}$$

# CONE FORM FACTOR IN THE CASE OF PANCAKE-LIKE OBJECTS

$$F_{\text{co}}(\varphi, \alpha_f) = \int_0^{H_{\text{co}}} Z_{\text{r}}^2(z, \psi_{\text{co}}) \frac{J_1(q_{\parallel}(\varphi, \alpha_f) \cdot Z_{\text{r}}(z, \psi_{\text{co}}))}{q_{\parallel}(\varphi, \alpha_f) \cdot Z_{\text{r}}(z, \psi_{\text{co}})} \exp\left(\frac{i}{2} q_z(\varphi, \alpha_f) z\right) dz$$

$$Z_{\text{r}}(z, \psi_{\text{co}}) = R_{\text{co}} - z / \cot \psi_{\text{co}}$$

$R_{\text{co}} = 150 \text{ nm}$   
 $H_{\text{co}} = 10 \text{ nm}$



$\psi_{\text{co}} = 0^\circ$

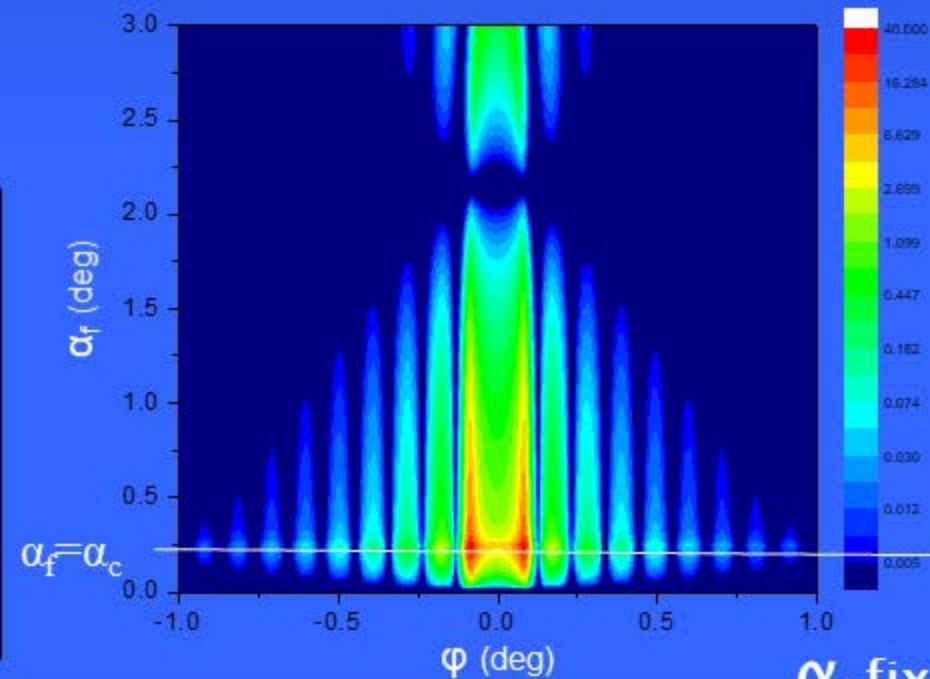
cylinder

$$|F_{\text{cy}}(\varphi, \alpha_f)| = \frac{J_1(q_{\parallel}(\varphi, \alpha_f) R) \sin(q_z(\varphi, \alpha_f) H/2)}{q_{\parallel}(\varphi, \alpha_f) R \quad q_z(\varphi, \alpha_f) H/2}$$

# CYLINDER FORM FACTOR AS SEEN IN THE 2d DETECTOR

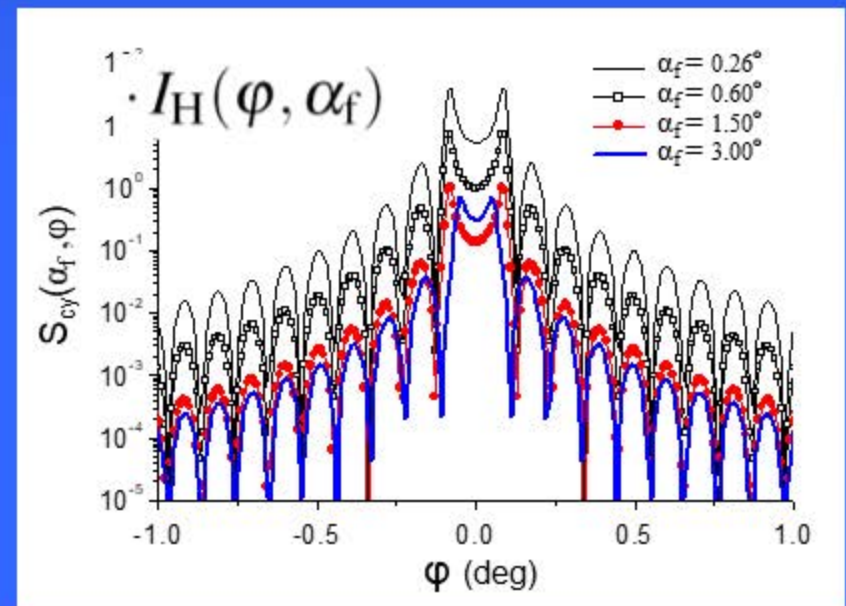
Specific of grazing incidence scattering: framing of the form-factor by the Fresnel transmission coefficients

$$S(q) = |F_{\text{BA}}|^2 \cdot T_i^2(\alpha_i) \cdot T_f^2(\alpha_f)$$



$\alpha_i$  fixed

$\alpha_f = \alpha_c$  fixed

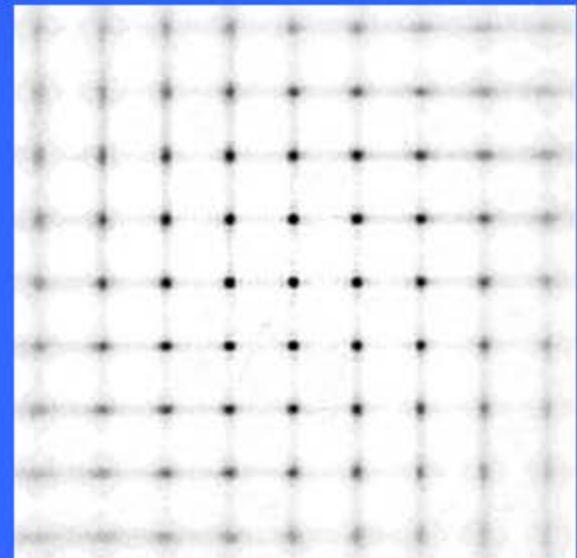


# DATA ANALYSIS IN SERGIS

Choice of the interference function – structure factor of one-dimensional ideal paracrystal (Hosemann and Bagchi)

$$I_H(\varphi, \alpha_f) = \frac{1 - e^{-q_{\parallel}(\varphi, \alpha_f)\sigma^2}}{1 + e^{-q_{\parallel}(\varphi, \alpha_f)\sigma^2} - 2e^{-\frac{1}{2}q_{\parallel}(\varphi, \alpha_f)\sigma^2} \cos(Dq_{\parallel}(\varphi, \alpha_f))}$$

D – the mean value of the lattice parameter  
 $\sigma$  – its standard deviation if the disorder factor obeys Gaussian distribution



Hosemann, R.; Bagchi, S. N. *Direct Analysis of Diffraction by Matter* (North-Holland Publishing Company: Amsterdam, 1962).

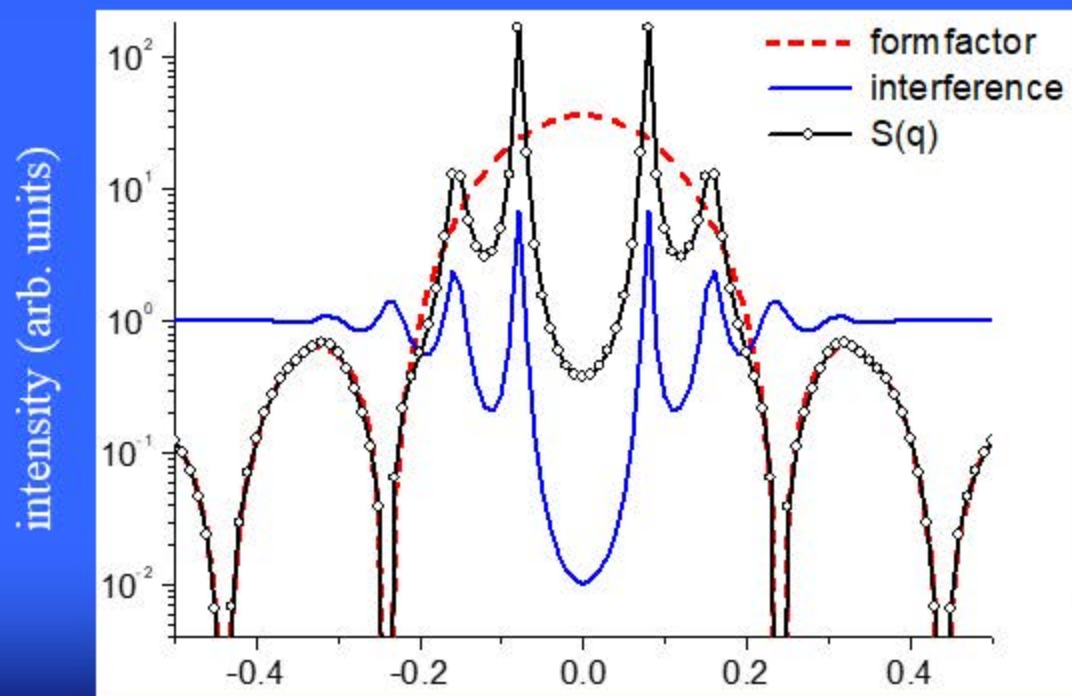
# SCATTERING INTENSITY DISTRIBUTION

$$S_{cy}(\varphi, \alpha_f) = M_c |F_{cy}(\varphi, \alpha_f)|^2 \cdot I_H(\varphi, \alpha_f)$$

$$|F_{cy}(\varphi, \alpha_f)| = \frac{J_1(q_{||}(\varphi, \alpha_f)R)}{q_{||}(\varphi, \alpha_f)R} \frac{\sin(q_z(\varphi, \alpha_f)H/2)}{q_z(\varphi, \alpha_f)H/2}$$



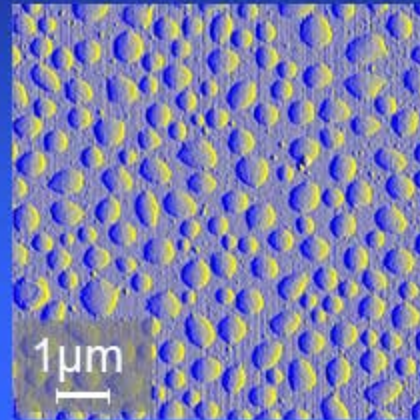
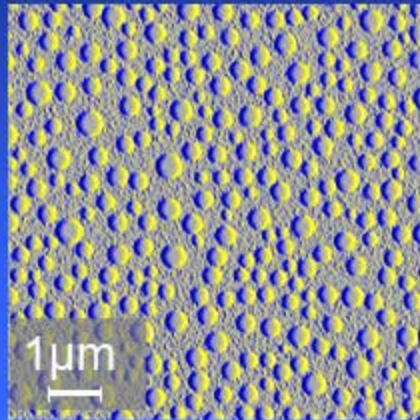
$$I_H(\varphi, \alpha_f) = \frac{1 - e^{-q_{||}(\varphi, \alpha_f)\sigma^2}}{1 + e^{-q_{||}(\varphi, \alpha_f)\sigma^2} - 2e^{-\frac{1}{2}q_{||}(\varphi, \alpha_f)\sigma^2} \cos(Dq_{||}(\varphi, \alpha_f))}$$



# COMPLIMENTARY DATA – AFM

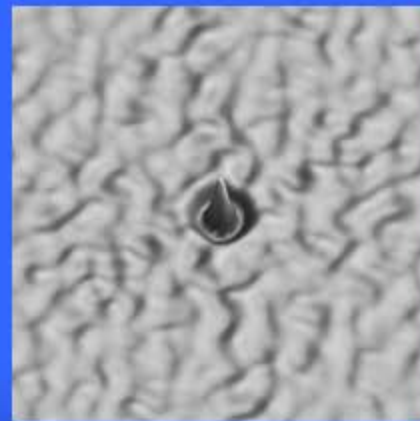
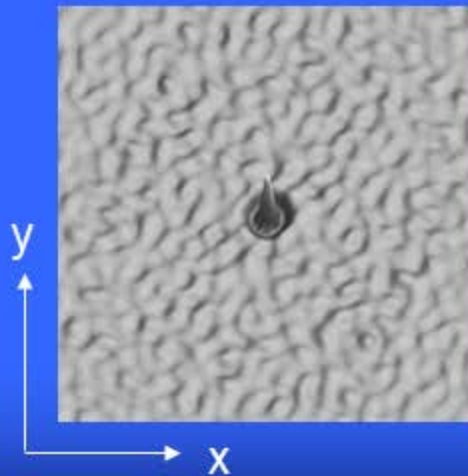
polymer blend

diblock copolymer

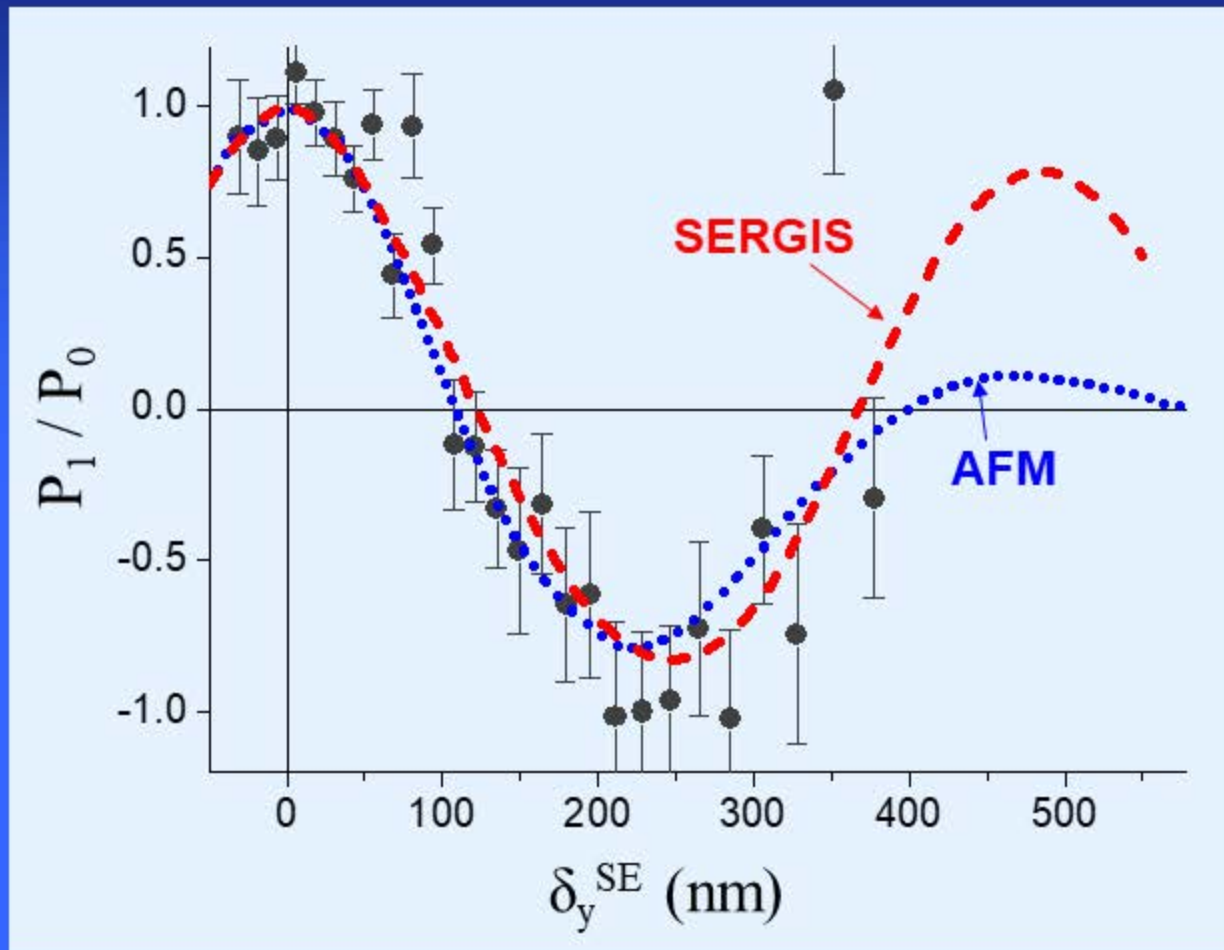


ACF

$$\Pi(\Delta a_1, \Delta a_2) = \sum \tilde{f}(a_1, a_2) \cdot \sum \tilde{f}(a_1 + \Delta a_1, a_2 + \Delta a_2)$$



# POLYMER BLEND



SERGIS  
model:

$R=170$  nm

$H=20$  nm

$D=480$  nm

$\sigma=50$  nm

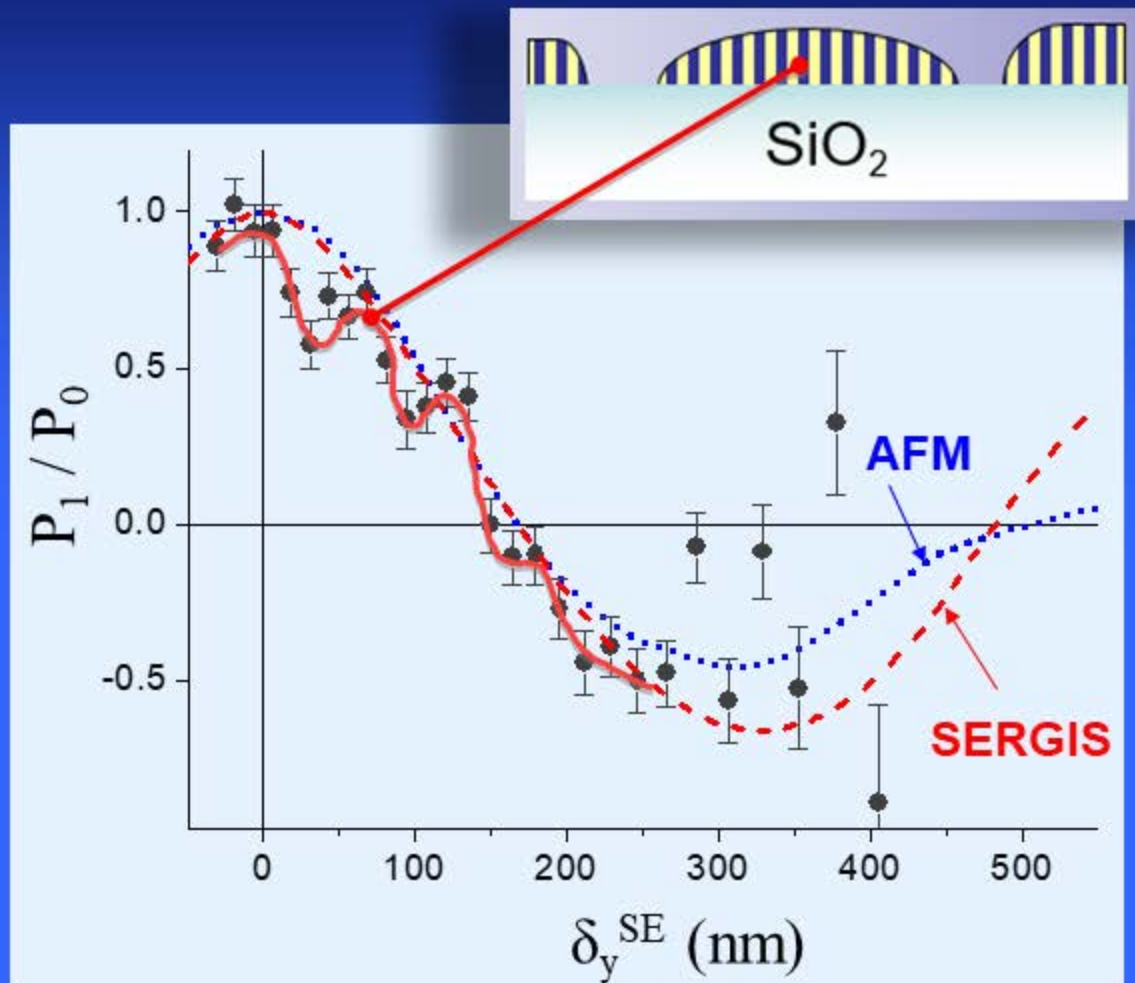
AFM:

$D=450$  nm

GISANS/GISAXS:

$D=500$  nm

# DIBLOCK COPOLYMER



SERGIS  
model:  
 $R=230$  nm  
 $H=10$  nm  
 $D=600$  nm  
 $\sigma/D=0.17$

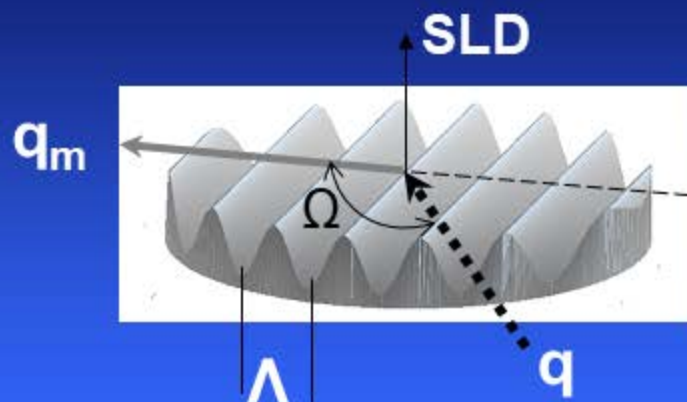
AFM:  
 $D=630$  nm

GISANS/GISAXS:  
 $D=600$  nm

AFM and X-rays can not see internal structure,  
GISANS can see and does see. What about SERGIS?



# MODULATED DROPLETS



SLD contrast

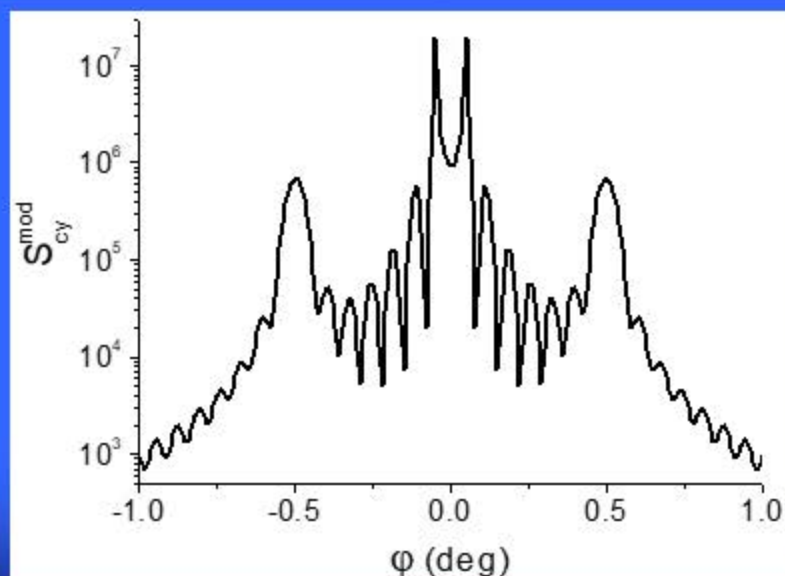
$$f_m(\mathbf{r}) = \bar{\rho} + \frac{\Delta\rho}{2} \cos(\mathbf{q}_m \cdot \mathbf{r})$$

mean SLD

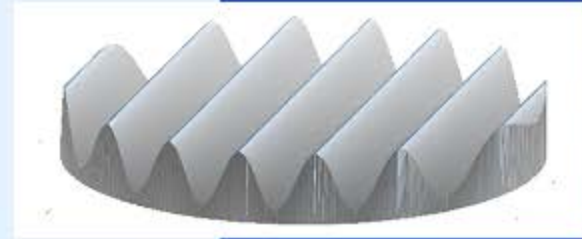
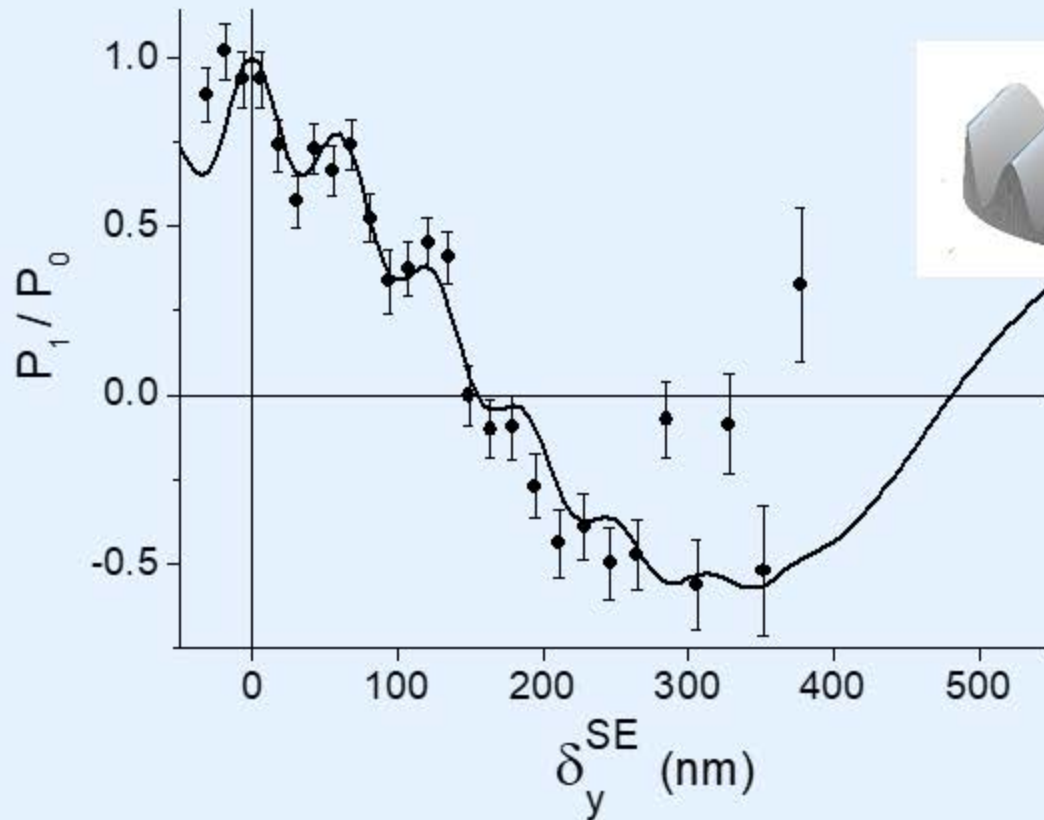
$$|F_{cy}^{\text{mod}}(\mathbf{q})| = \bar{\rho}|F_{cy}(\mathbf{q})| + \frac{\Delta\rho}{4} \left( \frac{J_1(|\mathbf{q}_{||} - \mathbf{q}_m|R)}{|\mathbf{q}_{||} - \mathbf{q}_m|R} + \frac{J_1(|\mathbf{q}_{||} + \mathbf{q}_m|R)}{|\mathbf{q}_{||} + \mathbf{q}_m|R} \right) \frac{\sin(q_z(\varphi, \alpha_f)H/2)}{q_z(\varphi, \alpha_f)H/2}$$

$$\overline{|F_{cy}^{\text{mod}}(\mathbf{q})|^2} = \frac{1}{\pi} \int_{-\pi/2}^{\pi/2} |F_{cy}^{\text{mod}}(\mathbf{q})|^2 d\Omega$$

$$S_{cy}^{\text{mod}}(\mathbf{q}) = c \overline{|F_{cy}^{\text{mod}}(\mathbf{q})|^2} I_H$$



# DIBLOCK COPOLYMER – MODULATED DROPLETS



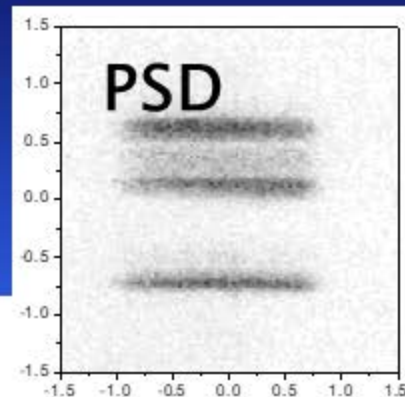
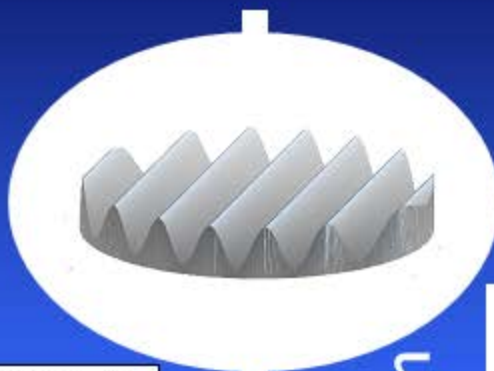
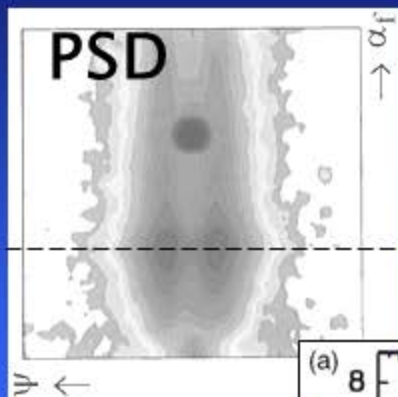
SERGIS  
 $\Lambda = 64$  nm

GISANS:  
 $\Lambda = 72$  nm

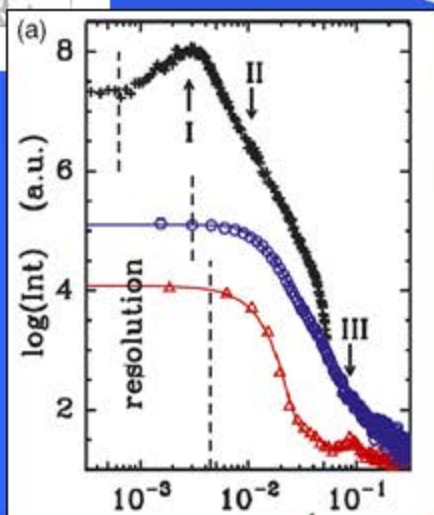
# GISANS

vs.

# SERGIS



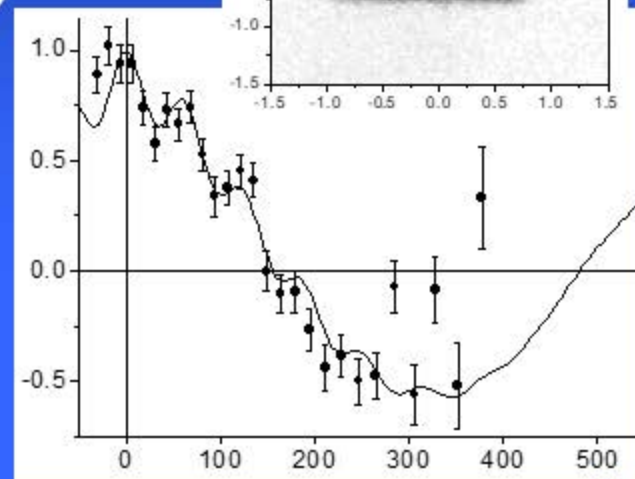
intensity



$\longrightarrow q_y \text{ (nm}^{-1}\text{)}$

measuring time  $T_m$ :  
8 hours at D22, ILL

polarization



$T_m$ : 12 h at EVA

improvements:

monochromator  $\Delta\lambda/\lambda$  5%  
 improved polarization circuit  
 improved measuring algorithm  
 (one component, less points)

time factor:

**12 h / 100  $\approx$  10 min**

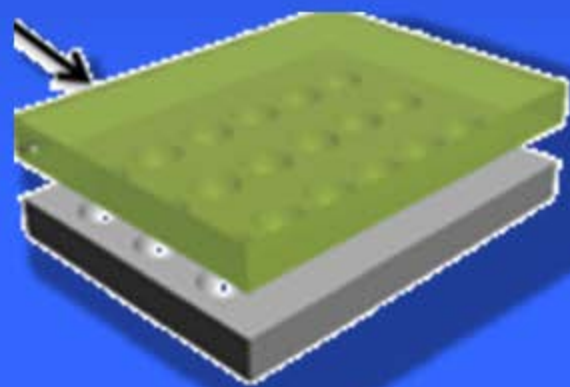
/5

/2

/10

# APPROPRIATE SAMPLES

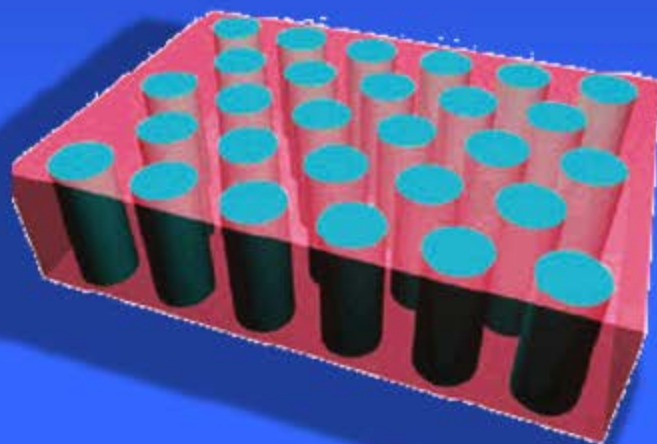
burred or fragile  
interface



cupping layer or liquid

~~SEM~~  
~~AFM~~

block copolymers



isotope contrast: D vs. H

# CONCLUSION

The SERGIS scattering technique can be especially advantageous for studying

- very soft or liquid surfaces
- buried interfaces

with length scales from few nanometers to few micrometers.

Due to the grazing angle geometry, structural information about surfaces/interfaces can be obtained with adjustable depth resolution.

*Phase and Microphase Separation of Polymer Thin Films  
Dewetted from Silicon – SERGIS Study*

A. Vorobiev et al.  
J. Phys. Chem. B **115** (2011) 5754-5765

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